#### PROJECT REPORT APPROVAL

The thesis titled "Effect of Existing Nearby Structures in Tunnel Excavation at TSC area" submitted by Fuad Bin Nazrul, Mohaimenul Islam, Mahdi Mansur and Mohammad Abu Umama, St. No. 155404, 155405,155422 and 155413 has been found as satisfactory and accepted as partial fulfillment of the requirement for the Degree Bachelor of Science in Civil Engineering.

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## Effect of Existing Nearby Structures in Tunnel Excavation at TSC Area

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Department of Civil and Environmental Engineering
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## A THESIS SUBMITTED FOR THE DEGREE OF BACHELOR OF SCIENCE IN CIVIL ENGINEERING

DEPARTMENT OF CIVIL AND ENVIRONMENTAL ENGINEERING
ISLAMIC UNIVERSITY OF TECHNOLOGY
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#### **DEDICATION**

Our combined thesis work is dedicated towards our respective parents, family and friends. We also express our gratitude the to our respected supervisor Professor Dr. Hossain Md. Shahin. This is a small token of appreciation towards all those who supported us throughout our endeavour and encouraged us to continue our work till the end.

#### **ACKNOWLEDGEMENTS**

"In the name of Allah, Most Gracious, Most Merciful"

All the praises to Allah (SWT) who has blessed us with the opportunity to complete this book. Our earnest gratitude towards our supervisor Professor Dr. Hossain Md. Shahin for giving us rightful instructions and for paying attention to us whenever needed throughout the research work. We are greatly indebted to him for enlightening us with his remarks and guidance in order to complete the thesis. Our sincere appreciation to Mozaher Ul Kabir and Musaddik Hossain, Lecturer, in the Department of Civil & Environmental Engineering, who have continuously guided us in our effort. We are also contended to Mahfuza Khanum, Geotechnical Engineer, Prosoil Foundation Consultant for her most valuable advice. We wish to show our gratefulness to 'Prosoil Foundation Consultant' for providing us necessary data extracted from soil investigation that they have performed previously. Our expression of gratitude towards all of the departmental faculty members for their aid and support.

We also appreciate all those individuals who have contributed in our work at any scale and those who have showered us with words of encouragement, inspiration and motivation. We are deeply obliged for the collaboration we have received throughout our work.

#### **ABSTRACT**

**Keywords:** Tunnel lining, Soil Parameters, Finite Element Method, Plaxis-2D, Surface Settlement, Numerical Analysis, Mohr Coulomb Model, Constitutive Model.

Urban underground structures e.g. construction of subway tunnels are a crucial part of Geotechnical Engineering. Existing nearby structures have a significant impact on construction and excavation work. Until starting the key construction sequences, proper investigation and accurate analysis are needed. This study addresses the TSC area tunnel project. Considering the impacts and risks associated with building loads, layout must be carried out. In this perspective, numerical analysis can be classified as an important tool to evaluate the ground deformations, surface settlements and stress that occurred during the tunnel construction sequences.

In this work, PLAXIS 2D, a finite element analysis application has been used to analyse finite elements. In the simulation Mohr Coulomb Model model has been used as a constitutive model of the soil. Laboratory tests have defined soil parameters that characterize physical and strength properties. Triaxial tests and consolidation tests obtained design parameters. It needs only a few integrated material parameters and can take into account the effect of the principal intermediate stress on soil deformation and strength, surface settlement, displacement vector, stress path influence on plastic flow direction and density and/or including pressure influence. It was found that the simulation of soil-structure interaction and behaviour according to the real life scenario in the Plaxis 2D system allows for higher safety factor. Therefore, with an advanced simulation tool Plaxis 2D, an advanced subway tunnel network can be designed for Dhaka city after proper ground movement prediction and tunnelling effect.

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#### **CHAPTER 1: INTRODUCTION**

#### 1.1 General

Tunneling has been widely used during the past decades. Due to the fast population growth and industrial activity, such type of infrastructures becomes a common technique in the urban area providing a wide range of facilities (transportation, electric line, ditches, etc.). To satisfy the increasing demand for tunneling advances in the technology of tunneling are necessary. For high-rise buildings supported by deep or shallow foundations, the construction of tunnel induces ground movements, which in turn affect the bearing capacity as well as the settlement of the existing foundations. To overcome this particular problem of the surface settlement many researchers have performed various tests to keep the settlement within allowable limits. Engineers are always concerned about the responses of soil behavior throughout the construction phases. A number of studies have been undertaken to understand the mechanisms of the soil— tunnel—pile interaction and to reduce the risk of possible adverse effects of tunneling on existing foundations. To ensure that excessive ground movement does not damage structures adjacent to tunnel constructions, care must be taken.

The interaction between loaded foundation and tunnel under construction is a three dimensional problem and modelling the influences of tunnel is only possible if tunneling-induced ground movements are assessed accurately. In practice the tunneling-induced ground movements are assessed by using empirical methods (Peck, 1969; Mair 1993; Clough and Schmidt, 1981; O'Reilly and New, 1982), analytical methods (Sagaseta, 1987; Verruijt and

Booker, 1996) and Finite element methods (Gunn, 1993; Rowe and Kack, 1983). Each method is subject to some limitations.

When the portion of the soil above the tunnel crown touches the tunnel lining, the soil at the side of the tunnel displaces towards the bottom of the tunnel. Therefore, the upward movement of the soil below the tunnel is limited. Centrifuge model tests carried out by Stallbrass et al. (1996) revealed similar results. Loganathan et al., (2001) assumed that about 75% of the vertical ground movement occurs within the upper annulus of the gap around the tunnel. (Ref: N. Loganathan, H. G. Poulos, K.J. Xu: Ground and Pile-group responses due to tunneling, Japanese Geotechnical Society, Japan)

For designing the tunnel lining engineers have to be concerned about the surrounding earth pressures of tunnel as well. Earth pressure in tunneling is usually estimated by using rigid plastic theory in which the deformation properties of the soil and the sequence of the excavation are not considered. In real cases, however, earth pressure depends on both properties of the ground and excavation sequences of tunnel. Elastic analysis also cannot properly explain such dependence of earth pressures in tunneling. Hence a more accurate deformation analyses is required to get realistic results of earth pressures. It is evident that meaningful numerical analysis can be made only If the stress distribution and density within the ground be predicted reliably. Therefore, a suitable constitutive model that the engineer can comprehend and apply easily is required. The constitutive model should consider typical soil behaviors including positive and negative dilatancy of soils, dependency of density and or confining pressure of soils. Mohr-Coulomb model is one of the constitutive models, which can describe different important characteristics of soils.

#### 1.2 Bacground

#### 1.2.1 Project Background

One of the largest growing megacities in the world is the capital of Bangladesh, Dhaka. The population is increasing every year inflicting serious problems like stagnant traffic condition throughout the city. Outdated traffic manoeuvring methods, lack of law-abiding tendencies, narrow road spaces are the main causes of elongated traffic jam situations. Economical losses that are sustained from these congestions are beyond negligence. It is also causing serious air pollution and noise pollution and thus worsens the overall environmental condition.

The plan of the subway in Dhaka city is not limited only in the plan or in paper. As per plan of the Government, the initiatives are being implemented and it will be done during this government. Government says the work of the subway project will be started during this government's tenure.

The Bangladesh Road Transport and Bridges Ministry and Spanish consulting body TYPSA have signed a contract for the construction of a subway system in Dhaka in July 2018. TYPSA, a leading consulting engineering group in transport, urban development, and renewable energy, will examine four possible routes for the subway. The first phase of construction for the subway will have an estimated cost of \$5.62 billion. Once completed, about 4 million out of around 8 million working population of Dhaka city would be able to use the underground subway on four routes and there will be a significant improvement in traffic condition of Dhaka city.

#### 1.2.2 Project Details

#### Primary selected proposed routes of subway in Dhaka:

- The first route will be around 32 kilometers in length; it will be from *Tongi Airport Kakali Mohakhali Moghbazar Paltan Motijheel Shapla Chattar – Sayedabad*, which will be extended to Narayanganj in the future. For this, the potential construction cost is estimated to be US\$ 5.66 billion.
- Secondly, a 16 km long subway line-2 will be from Aminbazar Gabtali Shyamoli
   Asadgate New Market TSC Ittefaq Moor Sayedabad. Later it will extend on both sides. The possible construction cost will be US\$ 2.87 billion.
- Thirdly, route-3 will be conducted from Gabtali Mirpur 1 Mirpur 10 Kakoli Gulshan 2 Natun Bazar Rampura TV Station Khilkhet Motijheel Shapla Chattar Jagannath Hall Keraniganj.
- Under route-4, the probability route of the subway will be from Rampura TV station –
   Niketan Tejgaon Sonargaon Hotel Panthapath Dhanmondi 27 Jigatala –
   Azimpur Lalbagh Sadarghat.

The length of root-3 and root-4 has not finalized yet. The underground depth of these subways will be from 20 to 40 meters. Sophisticated Tunnel Boring Machine (TBM) will be used to construct these subways. So, during the implementation of the project, people will not suffer due to dig on the soil.

In this particular study, TSC area is considered from the second route of the subway line. Proposed tunnel will be passing underneath the selected area. All the building loads are taken from Teacher Student Center (TSC) of Dhaka University. This building is the most nearby structure in the area.

#### References

- <a href="https://www.dhakatribune.com/bangladesh/communication/2018/08/03/subway-system-to-be-built-in-dhaka">https://www.dhakatribune.com/bangladesh/communication/2018/08/03/subway-system-to-be-built-in-dhaka</a>
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#### 1.2.3 Study Area



Figure 1.2.3.1: Study area (TSC area) from google map marked by red circle

There is a 50 ft wide road and from the footpath distance of the TSC building is 50 ft. From the soil report project "Feasibility Study and Preliminary Design for construction of Dhaka Subway" there is a borehole (BH 12) in TSC area which location is in X direction 234472.8125 and in Y direction 2627007.679. The foundation of TSC building is footing foundation.

#### 1.2.4 Technical Considerations

We have considered first two footing of TSC building at one section.

Footing	Length (ft)	Loading area (ft²)
First (Exterior)	4.5	144
Second (Interior)	8.0	216

Table 1.2.4.1 Footing details of TSC building

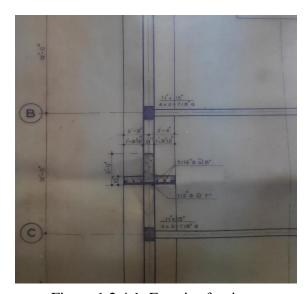


Figure 1.2.4.1: Exterior footing

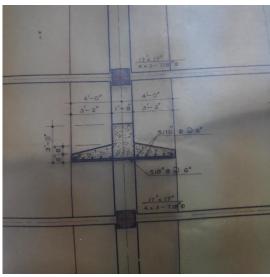


Figure 1.2.4.2: Interior footing

#### **Reference:**

• Plan view of TSC building, Engineering department of TSC building.

#### 1.2.5 Objectives

- Evaluating the effect of existing nearby structures in tunnel excavation
- Surface settlement induced by the existing structure and by the excavation of tunnel
- Determining the stress development on tunnel lining
- Water pressure and stress development due to the excavation of tunnel

#### **CHAPTER 2: LITERATURE REVIEW**

#### 2.1 Introduction

Around the world, there are many examples of subway tunnels. But this is a new technique in Bangladesh and very few studies have been done so far. PLAXIS 2D design has been used in this research to simulate subway tunnels for the proposed route under Dhaka City. The literature review was done to identify the studies related to this field that have been carried out already.

#### 2.2 Tunnel Construction

A tunnel construction method depends on ground and surface water conditions, excavation depth, surface loadings, tunnel drive length and diameter, tunnel lining width, tunnel excavation techniques, final use and tunnel structure etc.

For common uses, there are two basic forms of tunnel construction that are the following:

- 1. Cut and cover tunnels built in a shallow trench and then paved over
- 2. Bored tunnels, built in-situ, without scraping the above ground. Typically they are circular or horseshoe cross section known as shield tunneling.

#### 2.3 Past Research on Underground Tunneling System

□ Shahin et al. (2011) Conducted a study which proposed that the displacement applied at the tunnel crown greatly influences the surface settlement and the earth pressure around a tunnel for the same volume loss and the same surcharge.

zone of deformation. The maximum surface settlement happens beneath the existing structures. ☐ Ghaboussi et al. (1983) Stated that for similar situations the liner stresses generally decrease when radial displacements at the heading are allowed to take place prior to the ground and liner coming into contact. ☐ Mair and Taylor (1979) Observations from practice have shown that the distribution of the developing longitudinal settlement trough due to tunnel excavation is a s-likecurve. □ Shahin et al. (2016) Showed that due to the arching effect earth pressure decreases at the tunnel excavation boundary while excavating a single tunnel. ☐ Zhang et al. (2015) Analyzed the effect of multilayered soil on tunnel lining by using FEM. The relation between the numerical model and real measurement was convincing and satisfactory. ☐ Eric Leca (2007) The response of existing structures to tunneling induced ground movements depends on their geometry, construction type and overall structural condition. Typically, the construction of an unsupported tunnel opening in soft ground would generate large ground displacements which, in turn could lead to the formation of a failure zone behind the face. ☐ Meguid M. A. et al. (2002) To evaluate the effects of construction on the tunnels, it is important to assess the current state of stress in the lining so that incremental changes due to construction would not lead to stresses exceeding the allowable limits.

During tunneling loads from existing structures control the surface settlement and the

#### 2.4 Researches in perspective of Bangladesh:

Very few research work on the underground tunnelling network in Bangladesh has been carried out.

- Waheed et al. (2008) used the method of cut-and-cover excavation along the current railway crossings from Uttara junction to Kamalapur junction based on the traditional analysis process. In this situation, he suggested doing FEM.
- ☐ Farazandeh et al. (2010) reported that in Bangladesh's viewpoint, SHIELD tunnelling is the safest method.

#### **CHAPTER 3: METHODOLOGY**

#### 3.1 Methods of Analysis of tunneling system

There are generally two approaches to the analysis of a system. The first is the conventional analysis and the second is the Finite Element Method (FEM) numerical analysis. A numerical analysis or FEM developed numerical formulas and gives an accurate result based on computer programming.

#### 3.2 Numerical Analysis

Numerical analysis involves using approximation techniques to answer mathematical problems, taking into consideration the extent of possible errors. Although this analysis is an approximation, it is possible to produce results as accurately as desired.

In geotechnical engineering, numerical analysis is commonly used for the following:

- The simulation process is fast and simple to perform.
- The analysis is more reliable and realistic.
- Practically understanding and determining structural behaviour.
- The best analytical approach is to look at each structural behavioural step of the construction process.
- Resolve non-linear equation roots.
- Solve large equation systems.
- In this form of analysis, soil-structure interaction is adequately accounted for.
- In this study, interaction between soil and water can be modelled accurately.
- It is possible to accurately assess the settlement and deformation of the soil and structures.

Using PLAXIS 2D (2019 Version) software for numerical analysis there are several steps. In general settings we define the section. In definition of soil stratigraphy we set the soil parameters and in definition of the structural elements we define the footing, tunnel lining, plates parameters. Basically for numerical analysis there are 5 phases. Phase 1: Building, Phase 2: Tunnel, Phase 3: Contraction, Phase 4: Grouting, Phase 5: Final Lining.

#### 3.3 Finite Element Method (FEM)

With different analytical method it cannot be solved irregular structures accurately. But using Finite Element Method (FEM), one can solve irregular structures accurately and easily. According to O. O. Ochoa and J. N. Reddy, Finite Element Analysis of Composite Laminates , 2nd ed. (1992) FEM has two features that no other method shares-

- The domain of the problem is represented by a collection of simple sub-domains, called finite elements. The subdivision of a domain into elements is termed finite element discretization. The collection of finite elements is called finite element mesh.
- ii. Over each finite element, the solution of the governing equations is approximated by a linear combination of undetermined parameters and preselected approximation functions, almost always polynomials. Since the solutions is represented by polynomial on each element, a continuous approximation of the solution of the whole can be obtained only by imposing the continuity of the element solution and possibly its derivatives, at element interfaces. The procedure of putting the elements together is called the assembly of elements.

The algebraic equations relating physical quantities at selective points, called nodes. (J. N. Reddy, An Introduction to the Finite Element Method, 3rd ed.(2005))

The solution of the element analysis and the system analysis is required for Finite Element Method (FEM). The relationship between nodal forces and nodal displacements from equilibrium conditions at nodes in element analysis is expressed in terms of a stiffness matrix for the element. A system of equilibrium equations come from assembling all individual elements to form the complete structure from the stiffness matrices.

Then application of the prescribed boundary conditions to solve these equilibrium equations.

The method gives sufficiently accurate results when the selected displacement patterns for the elements are able to produce constant stress fields inside the elements.

In this research, using PLAXIS 2D (software version 2019) two-dimensional finite element analyses have been carried out. Soil ground is divided into a certain number of elements with six nodes. For simplicity, considering plane strain condition for 2D Ground Model.

#### 3.4 Soil Model

There are various kinds of soil model in PLAXIS 2D. The name of the soil models are:

- Linear Elastic Model (LE)
- Mohr-Coulomb Model (MC)
- Hardening Soil Model (HS)
- Hardening Soil Model with small stress-strain stiffness (HS small)
- Soft Soil Model (SS)
- Soft Soil Creep Model (SSC)
- Jointed Rock Model (JR)
- Modified Cam-Clay Model (MCC)
- NGI-ADP Model (NGI-ADP)
- UDCAM-S Model (UDCAM-S)
- Sekivguchi-Ohta Model (Seki guchi-Ohta)
- Hoek-Brown Model (HB)
- UBC3D-PLM Model (UBC3D-PLM)
- Concrete Model (Concrete)

In this research work, materials are modelled with Mohr Coulomb model in PLAXIS 2D software. This model has some advantages over other soil model:

Straightforward method for soils and it is simpler in Mathematical expression.	
It's physical quantities more clearly understandable.	

## CHAPTER 4: MODEL CONSIDERATIONS, TUNNEL GEOMETRY AND SOIL BOUNDARY

#### 4.1 Introduction

Based	on the literature review following considerations have been taken
	Finite Element Modelling of Tunnel Excavation
	Nearby Existing Structure
4.2 Se	election of Construction Method
	Plania 2D Caferra a 2010 annia
ч	Plaxis 2D Software 2019 version
	Consider element with 6 nodes
	Consider plane strain condition for 2D Ground Model
	Materials are modelled with Mohr Coulomb model
	Microsoft Excel for generating tables and graphs
	AutoCAD 2016 for drawing figures.
4.3 T	unnel Geometry
	Tunnel depth: Tunnel crown is 33 meter down from the surface of the soil
	Tunnel diameter (B): 11 meter
	Tunnel centre: (10.5B, 3.5B) or (115.5,38.5) from the left side of the section
	Contraction: 5%

#### 4.4 Lining and Footing

□ Lining Thickness: 0.35 meter (From global database of PLAXIS 2D)
 □ Lining bending modulus (EI): 14.3x10<sup>4</sup> kN/m²/m (From global database of PLAXIS 2D)
 □ Lining axial modulus (EA): 14x10<sup>6</sup> kN/m (From global database of PLAXIS 2D)
 □ Lining other values: From global database of PLAXIS 2D
 □ Footing bending modulus (EI): 24x10<sup>3</sup> kN/m²/m (From global database of PLAXIS 2D)
 □ Footing axial modulus (EA): 7.6x10<sup>6</sup> kN/m (From global database of PLAXIS 2D)
 □ Footing other values: From global database of PLAXIS 2D

#### **4.5 Section Geometry**

☐ Section type : Two dimensional

 $\square$  Length: 10B+B+10B=21B=231 meter (Where tunnel diameter, B=11 meter)

 $\square$  Depth: 6B = 66 meter (Where tunnel diameter, B = 11 meter)

#### 4.6 Soil Parameters

Soil sample are collected from TSC area (Borehole 12) and the parameters are considered as the basic design input for the model. Soil parameters are extracted from the USCS soil classification, SPT values and different co-relations. From the soil report of Prosoil Foundation Consultant we get different important parameters for different co-relation.

#### Following tests are performed:

- i. Particle size analysis-sieve
- ii. Particle size analysis-Hydrometer
- iii. Atterberg limits test
- iv. Natural moisture content
- v. Dry and apparent density
- vi. Particle density
- vii. Unconfined compressive strength
- viii. Triaxial test (CU)
- ix. Consolidation test



Figure 4.6.1: Tri-axial test at Prosoil Foundation Consultant laboratory

Layers			Borehole_TSC		
#	Material		Тор	Bottom	
1		Layer 1	0.000	-3.750	
2		Layer 2	-3.750	-6.750	
3		Layer 3	-6.750	-9.750	
4		Layer 4	-9.750	-11.75	
5		Layer 5	-11.75	-28.00	
6		Layer 6	-28.00	-60.00	

Figure 4.6.2: Borelog of the model (From PLAXIS 2D software)

#### **Basic parameters:**

**E** = **Modulus** of elasticity

**C** = **Cohesion** 

 $\Phi$  = Angle of internal friction

v = Poisson's ratio.

 $\Psi$  = Angle of dilatancy

From the soil report we get Standard penetration test (SPT) values for different depth. We took the average of them then modified it close to the lowest value. Then from USCS soil classification and different co-relation from books we get the soil parameters.

For simplicity we have considered the soil as pure clay r pure sand. But in clay soil we gave angle of friction value 1 degree for make in Undrained B condition in the software.

Layer	Depth (m)	Classification of soil (USCS)	Description	Avg SPT	Modulus of elasticity (E) MPa	Cohesion (c) Kpa	Angle of friction $(\Phi)$ Degree	Angle of dilatancy (Y) Degree	Poisson's Ratio (υ)
1	0.00 to 3.75	CL	Reddish Brown, medium stiff to stiff, Lean Clay	5	9	30	1	0	0.4
2	3.75 to 6.75	СН	Reddish Brown, stiff to very stiff, Fat Clay	13	14	65	1	0	0.4
3	6.75 to 9.75	CL	Reddish Brown, stiff to very stiff, Lean Clay	12	12	60	1	0	0.4
4	9.75 to 11.75	CL	Reddish Brown, very stiff, Sandy Lean Clay	22	30	80	1	0	0.4
5	11.75 to 28	SM	Brown,medium dense to very dense,Silty Sand	24	20	0	31	1	0.3
6	28 to 66	SM	Brown,medium dense to very dense,Silty Sand	57	30	0	34	4	0.3

Table 4.6.1 : Basic parameters of soil for model simulation.

#### **4.7 Load Calculation**

For estimating the footing load we have considered the service load only.

Service Load = Dead Load + Live Load

From BNBC 2006 we took the values of Dead Load and Live Load for TSC building.

Dead Load:					
Weight of all materials of construction incorporated into the building					
Mat	erial	Weight per un	it area(kN/m²)		
Floor (Concrete slab)	solid, 150 mm thick	3.5	540		
Roof concrete	, 25 mm thick	0.5	527		
Walls and Partitions s	and-lime, per 100 mm	2.4	75		
Ceiling Cement pl	aster, 13 mm thick	0.287			
Miscellaneous Plaste	•	0.230			
	Live Loads for Va	rious Occupancies			
Building	Occupancy	Use of floor	Weight per unit area (kN/m²)		
Educational,		Class room, lecture			
Institutional B,C,D Building		room, lounge.	3.0		

Table 4.6.2 : Dead Loads and Live Loads occurring in TSC building.

#### Calculation of load for the exterior footing:

Number of floor = 4

Footing length = 4.5 ft = 1.3716 m

Loading area =  $144 \text{ ft}^2 = 13.3780 \text{ m}^2$ 

Service load = Dead Load + Live Load =  $10.059 \text{ kN/m}^2$ 

Load acting on the exterior footing = (4\*10.059\*13.3780) kN = 538.2772 kN

So, in exterior footing load acting per length = (538.2772/1.3716) = 392.4447 kN

#### Calculation of load for the interior footing:

Number of floor = 4

Footing length = 8 ft = 2.4384 m

Loading area =  $216 \text{ ft}^2 = 20.0671 \text{ m}^2$ 

Service load = Dead Load + Live Load =  $10.059 \text{ kN/m}^2$ 

Load acting on the exterior footing = (4\*10.059\*20.0671) kN = 807.418091 kN

So, in exterior footing load acting per length = (807.418091/2.4384) = 332.1261 kN

#### 4.8 Mesh Generation

There are different types of finite element meshes in PLAXIS 2D software for FEM analysis.

For meshing we have used element distribution very fine.

#### 4.9 Displacement Boundary and Water table

#### 4.9.1 Displacement Boundary

The displacement boundary conditions are as follows:

At bottom: Both vertical and horizontal displacements are fixed.

At left edge: The horizontal displacement is fixed but vertical movement is allowed; i.e., vertical displacement is pinned.

At right edge: The horizontal displacement is fixed but vertical movement is allowed; i.e., vertical displacement is pinned.

#### 4.9.2 Water table

Water table is at the top of the soil layer (from the borelog of the soil report).

#### **4.10 Cases Considerations**

In this research work we have considered two cases.

CASE 1	Tunnel under 1 <sup>st</sup> footing of the building
CASE 2	Tunnel under the center of the road (22.86m distance from CASE 1)

Table 4.10.1: Cases that has been considered

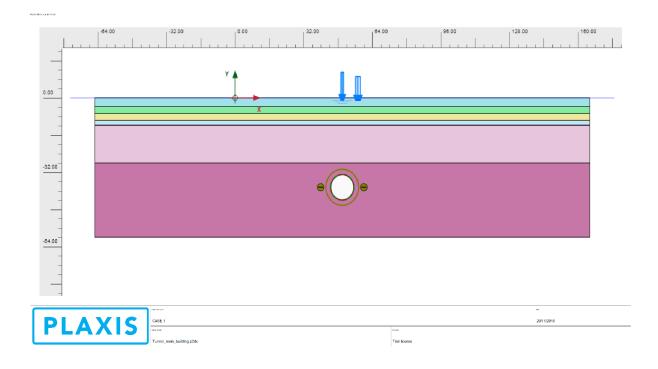


Figure 4.10.1 : CASE 1 – Tunnel under 1<sup>st</sup> footing of the building

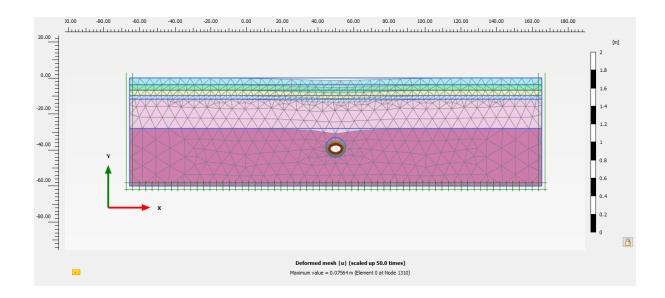


Figure 4.10.2 : CASE 2 – Tunnel under center of the road (22.86m distance from CASE 1)

#### **CHAPTER 5: RESULTS AND DISCUSSIONS**

#### 5.1 Introduction

Results of different cases and scenarios are mentioned in this section:

The deformed mesh, total displacement, horizontal displacement, vertical displacement of soil behaviour and bending moment, shear force, axial force for tunnel behaviour are mentioned in this section.

For this research work we have moved the tunnel by 10 meter repeatedly. So, we have got 6 scenarios. Total nine scenarios we have got considering tunnel without any surface load, CASE 1 and CASE 2.

#### **5.2 Ground Condition**

#### **5.2.1 Deformed mesh**

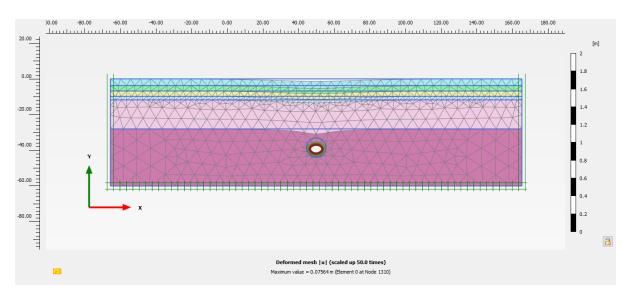


Figure 5.2.1.1: Deformed mesh (Tunnel without any existing structure)

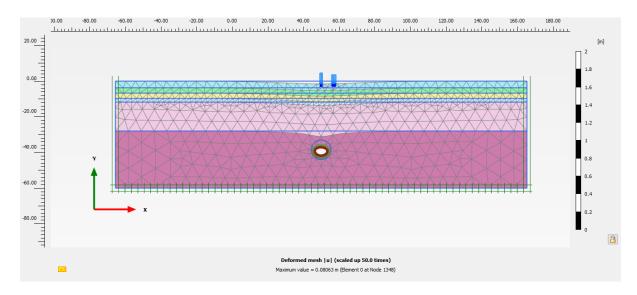


Figure 5.2.1.2: Deformed mesh (CASE 1 - Tunnel under 1st footing of the building)

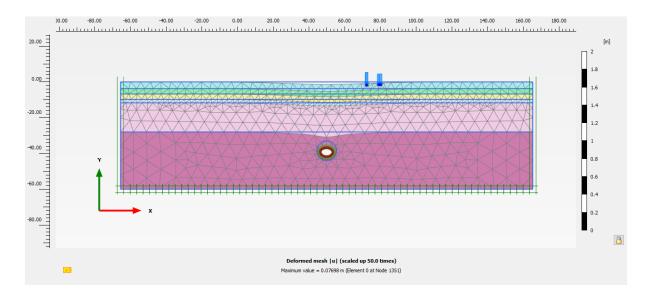


Figure 5.2.1.3: Deformed mesh (CASE 2 – Tunnel under center of the road)

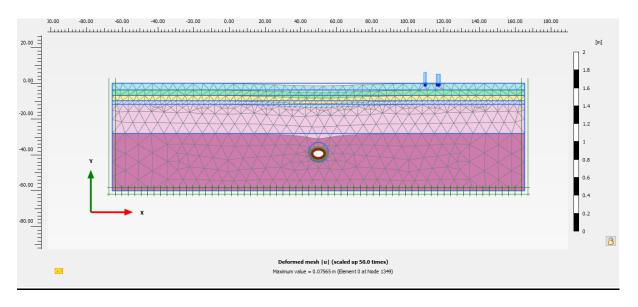


Figure 5.2.1.4: Deformed mesh (Tunnel at 60m distance from CASE 1)

## **5.2.2** Total displacement

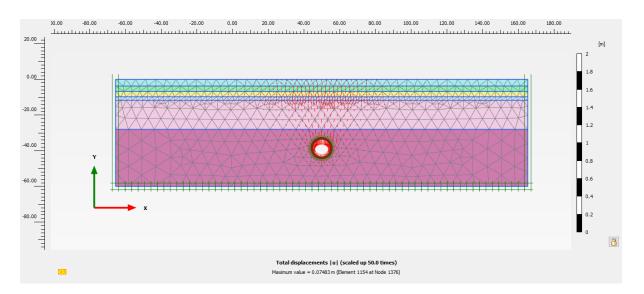


Figure 5.2.2.1.: Total displacement (Tunnel without any existing structure)

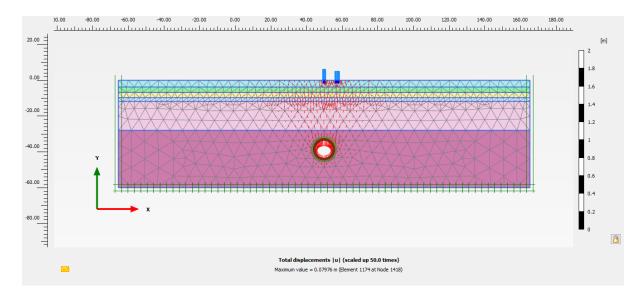


Figure 5.2.2.2: Total displacement (CASE 1 - Tunnel under 1st footing of the building)

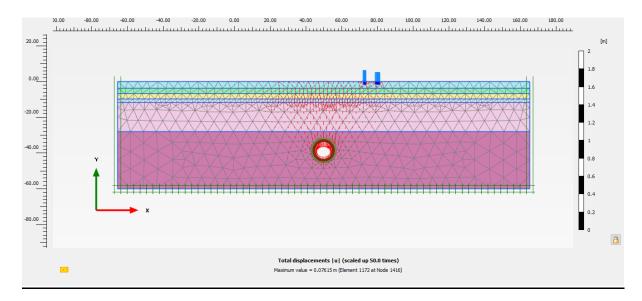


Figure 5.2.2.3: Total displacement (CASE 2 – Tunnel under center of the road)

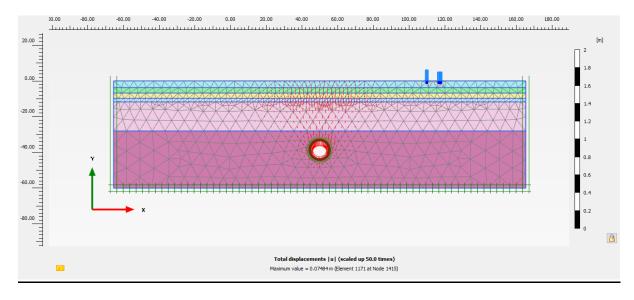


Figure 5.2.2.4: Total displacement (Tunnel at 60m distance from CASE 1)

# 5.2.3 Horizontal displacement

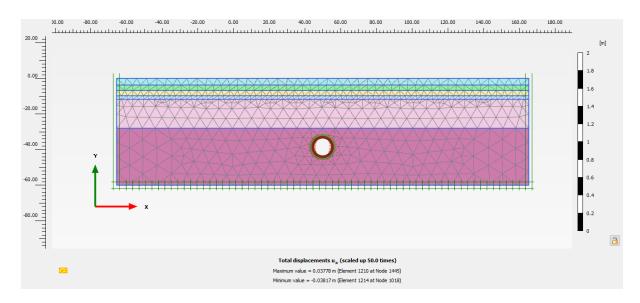


Figure 5.2.3.1: Horizontal displacement (Tunnel without any existing structure)

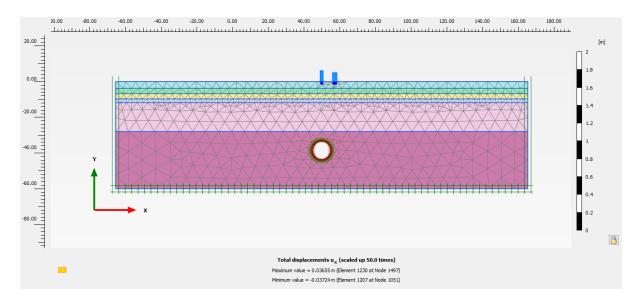


Figure 5.2.3.2: Horizontal displacement (CASE 1 - Tunnel under 1st footing of the building)

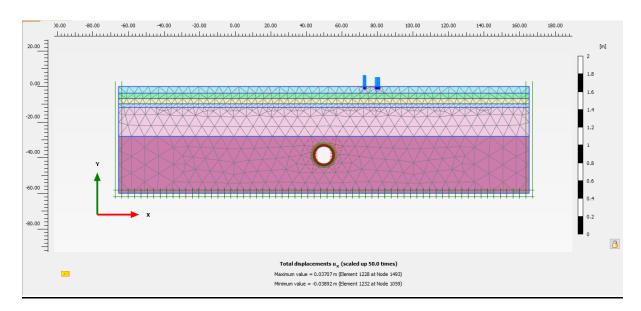


Figure 5.2.3.3: Horizontal displacement (CASE 2 – Tunnel under center of the road)

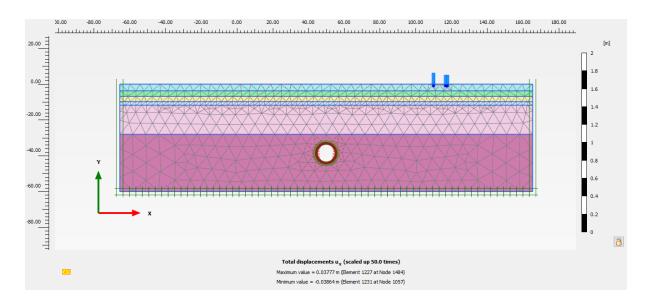


Figure 5.2.3.4: Horizontal displacement (Tunnel at 60m distance from CASE 1)

## **5.2.4 Vertical Displacement**

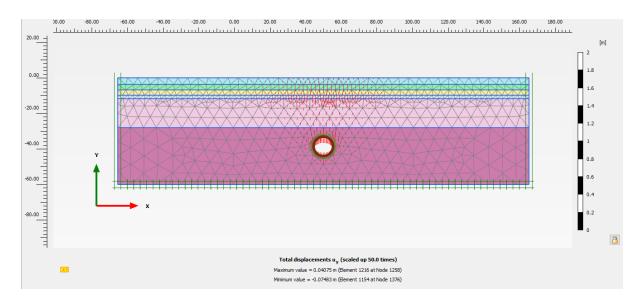


Figure 5.2.4.1: Vertical displacement (Tunnel without any existing structure)

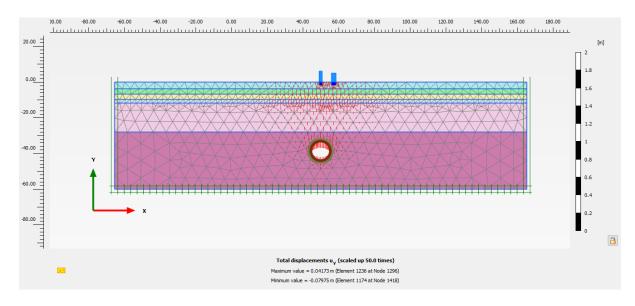


Figure 5.2.4.2: Vertical displacement (CASE 1 - Tunnel under 1st footing of the building)

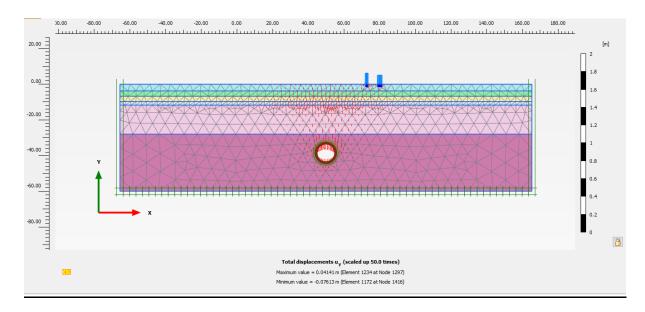


Figure 5.2.4.3: Vertical displacement (CASE 2 – Tunnel under center of the road)

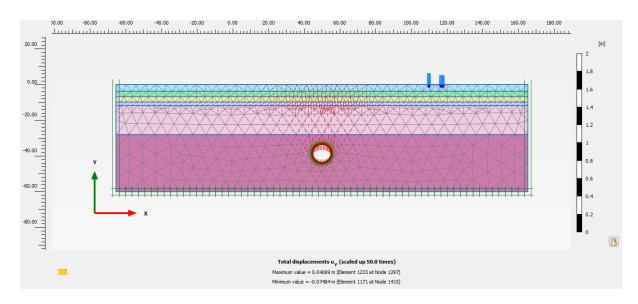


Figure 5.2.4.4: Vertical displacement (Tunnel at 60m distance from CASE 1)

## **5.3 Tunnel lining condition**

# **5.3.1 Bending Moment**

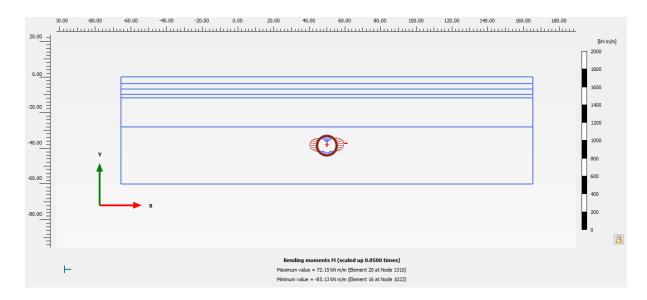


Figure 5.3.1.1: Bending moment diagram of tunnel (Tunnel without any existing structure)

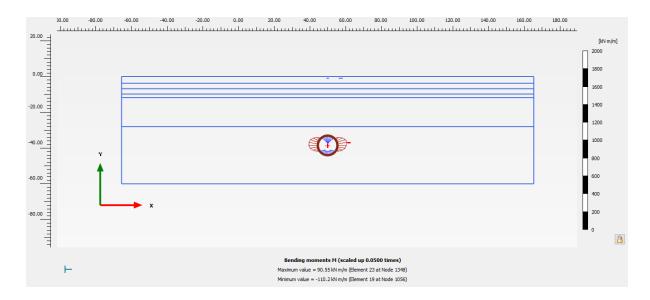


Figure 5.3.1.2: Bending moment diagram of tunnel (CASE 1)

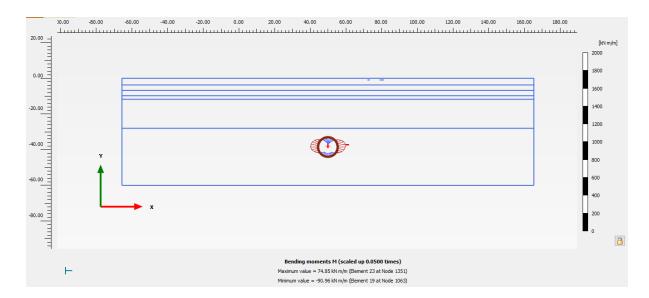


Figure 5.3.1.3: Bending moment diagram of tunnel (CASE 2)

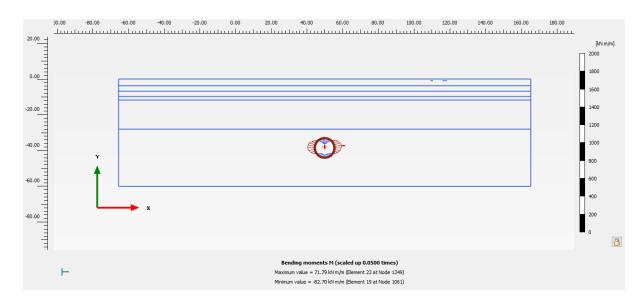


Figure 5.3.1.4: Bending moment diagram of tunnel (Tunnel at 60m distance from CASE 1)

#### **5.3.2** Shear force

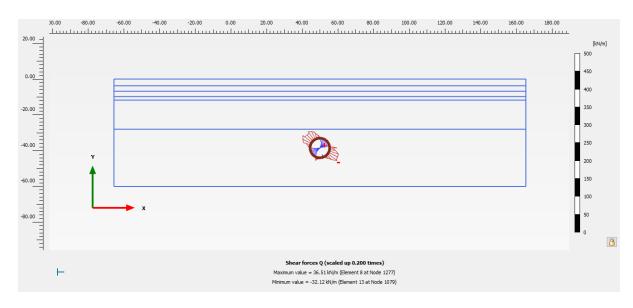


Figure 5.3.2.1: Shear force diagram of tunnel (Tunnel without any existing structure)

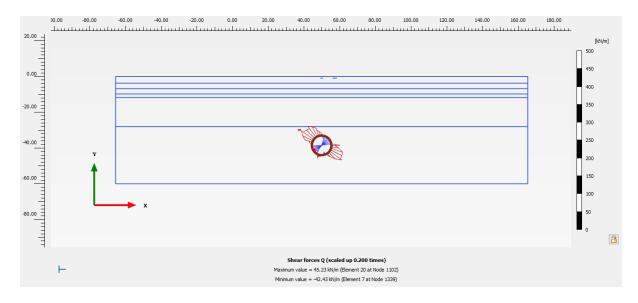


Figure 5.3.2.2: Shear force diagram of tunnel (CASE 1)

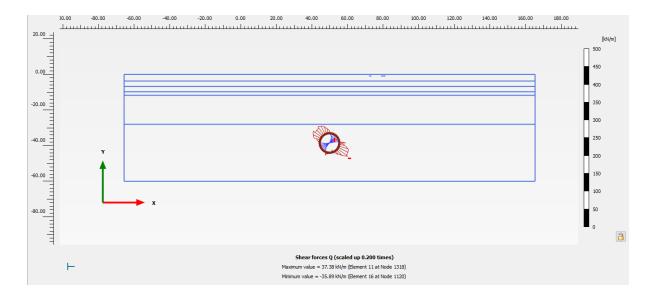


Figure 5.3.2.3: Shear force diagram of tunnel (CASE 2 – Tunnel under center of the road)

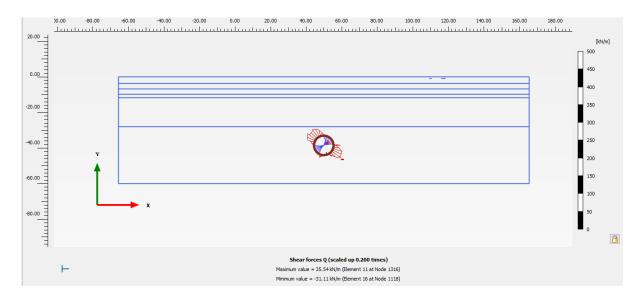


Figure 5.3.2.4: Shear force diagram of tunnel (Tunnel at 60m distance from CASE 1)

#### 5.3.3 Axial force

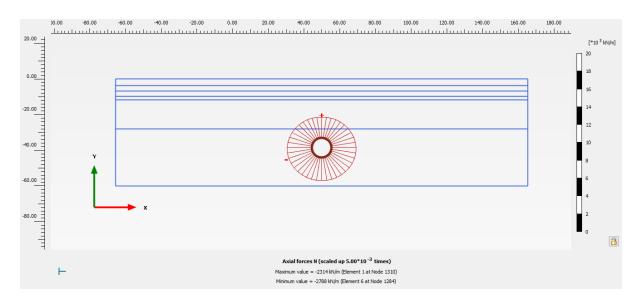


Figure 5.3.3.1: Axial force diagram of tunnel (Tunnel without any existing structure)

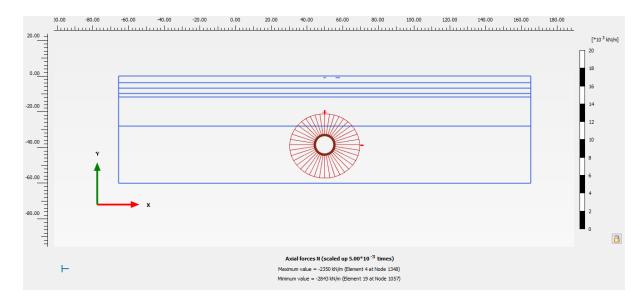


Figure 5.3.3.2: Axial force diagram of tunnel (CASE 1)

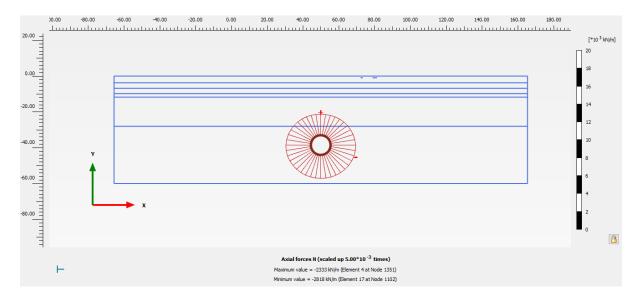


Figure 5.3.3.3: Axial force diagram of tunnel (CASE 2 – Tunnel under center of the road)

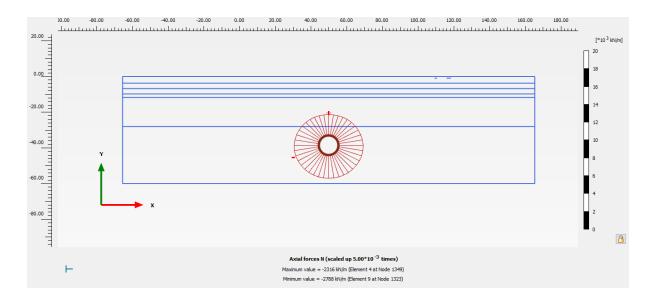
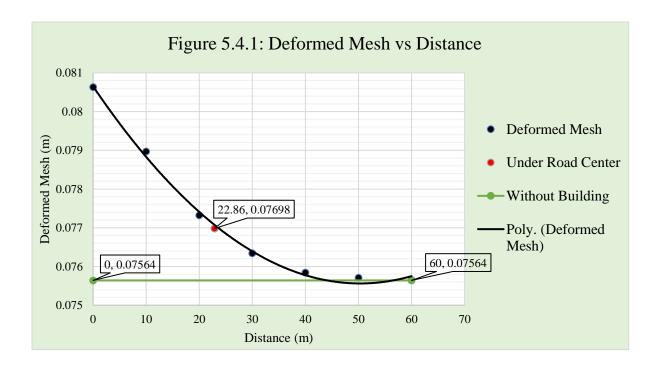
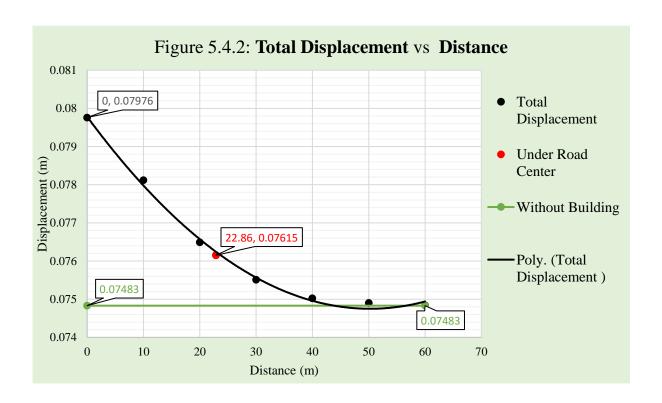
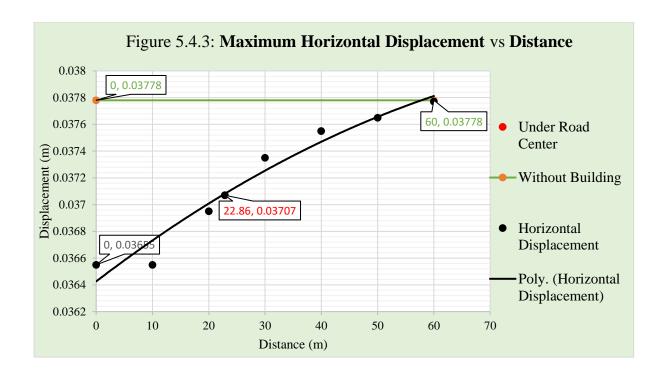


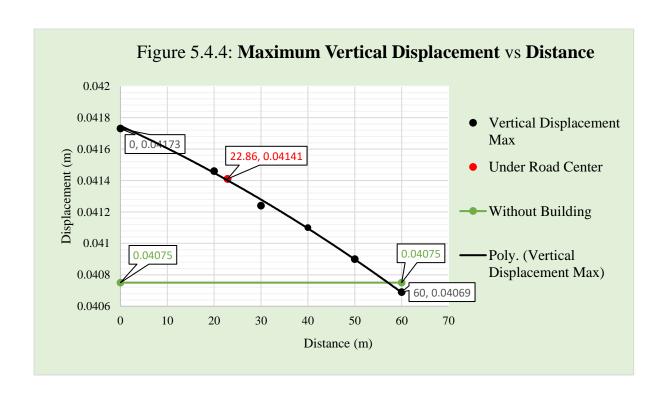
Figure 5.3.3.4: Axial force diagram of tunnel (Tunnel at 60m distance from CASE 1)

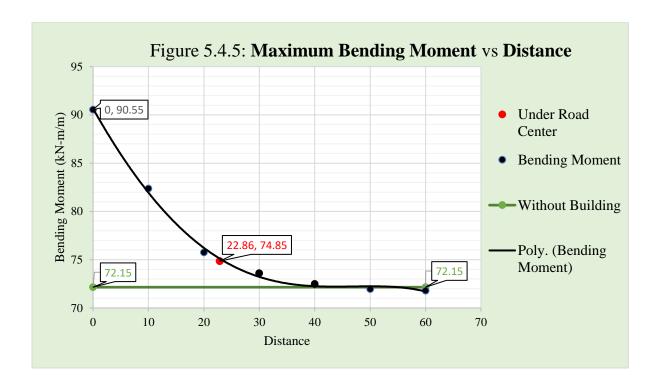
#### 5.4 Graphs



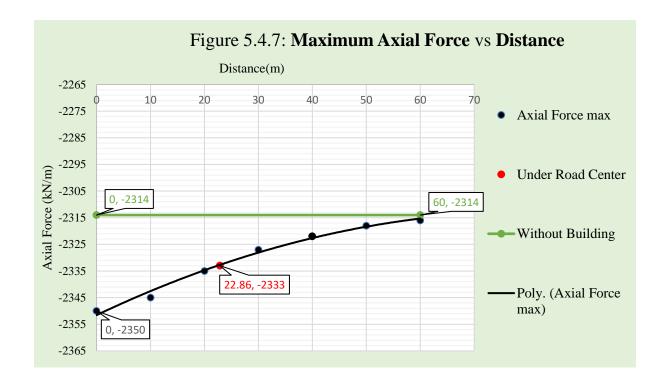












#### 5.5 Discussion

From the results we can discuss that if we consider the base values are for all conditions (ground and tunnel lining) the values extract from the tunnel without any surface load for every cases then most of the condition's values meets the base values ((Tunnel at 60m distance from CASE 1).

Conditions		Tunnel			Tunnel at	
		without			60m	
			CASE 1	CASE 2	distance	Comment
		surface			from	
		load			CASE 1	
Ground	Deformed mesh	0.07564	0.08063	0.07698	0.07565	Very close
condition	(m)	0.0700.	0.0000	0.07020	0.0,000	, ory cross
	Total	.07483	0.07976	0.07615	0.07484	Very close
	Displacement(m)	.07403	0.01710	0.07976 0.07615		very close
	Horizontal					
	displacement	.03778	0.03655	0.03707	0.03777	Very close
	(m)					
	Vertical					Closely
	displacement	.04075	0.04173	0.04141	0.04069	enough
	(m)					chough
Tunnel	Bending moment	72.15	90.55	74.85	71.70	Closely
lining	(kN-m/m)	72.15			71.79	enough
condition	Shear force	36.51			25.54	Meets
	(kN/m) Axial		45.23	37.38	35.54	early
			-2350	-2333	-2316	Very close
	force(kN/m)	-2314	2330	2333	2310	, cry crose

Table 5.5.1: Results and comments for all scenarios

There were some limitations and unwanted shapes in the graphs for creating the best line curves. Some values were unrealistic. Because of

- Soil parameters are extracted from USCS soil classification, SPT values and different co-relations.
- The modelled soil parameter was not similar to the actual field soil parameters.
- The plates and tunnel lining data are collected from global database of PLAXIS 2D software.

# CHAPTER 6: CONLUSIONS AND RECOMMENDATIONS

#### **6.1 Conclusions**

Similarities were found in soil behavior and tunnel lining behavior between the initial
condition(without nearby structure) and moving the tunnel around 60 m from the initial
phase.(CASE 1)
For case 2, tunnel is suggested to be moved around 37.14m.
In case of similar soil layers, similar ground behavior can be speculated in tunnel
construction in Dhaka city.

#### **6.2 Future work and recommendations**

- In this study we have considered only the distance of tunnel where there was no effect of surface loading. A proposal can be made on lining thickness of the tunnel in future.
- We have used the modified soil parameters. In future using real field data is suggested.
- In future instead of using Mohr-Coulomb criteria, other material models e.g. Hardening Soil Model, Soft Soil Model etc. can be used and compared with various models.
- In our study we have considered the 2D effect only. But in future3D effect of soil and tunnel lining behaviour can be an advanced topic of research for this project.
- Finally, though parametric values are obtained from SPT, in case of accuracy of the model Triaxial test is suggested.

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#### **APPENDIX A**

The result and values for different scenarios

Tunnel without any surface loading						
Deformed Mesh (m)	Total Displacement (m)	Horizontal Displacement Maximum (m)	Vertical Displacement Maximum (m)	Bending moment Maximum (kN-m/m)	Shear Force Maximum (kN/m)	Axial Force maximum (kN/m)
0.07564	0.07483	0.03778	0.04075	72.15	36.51	-2314

	CASE 1 - Tunnel under 1st footing of the building						
Deformed Mesh (m)	Total Displacement (m)	Horizontal Displacement Maximum (m)	Vertical Displacement Maximum (m)	Bending moment Maximum (kN-m/m)	Shear Force Maximum (kN/m)	Axial Force maximum (kN/m)	
0.08063	0.07976	0.03655	0.04173	90.55	45.23	-2350	

CASE 2 - Tunnel under the center of the road (22.86m distance from CASE 1)						
Deformed Mesh (m)	Total Displacement (m)	Horizontal Displacement Maximum (m)	Vertical Displacement Maximum (m)	Bending moment Maximum (kN-m/m)	Shear Force Maximum (kN/m)	Axial Force maximum (kN/m)
0.07698	0.07615	0.03707	0.04141	74.85	37.38	-2333

Tunnel has been moved 10 meters repeatedly. So, we get 6 scenarios.

	Tunnel moved from CASE 1							
Tunnel movement distance (m)	Deformed Mesh (m)	Total Displacement (m)	Horizontal Displacement Maximum (m)	Vertical Displacement Maximum (m)	Bending moment Maximum (kN-m/m)	Shear Force Maximum (kN/m)	Axial Force maximum (kN/m)	
0	0.08063	0.07976	0.03655	0.04173	90.55	45.23	-2350	
10	0.07897	0.07812	0.03655	0.04163	82.38	43.11	-2345	
20	0.07732	0.07649	0.03695	0.04146	75.75	39.05	-2335	
30	0.07634	0.07551	0.03735	0.04124	73.6	37.2	-2327	
40	0.07584	0.07502	0.03755	0.0411	72.48	37.1	-2322	
50	0.07571	0.0749	0.03765	0.0409	71.96	36.8	-2318	
60	0.07565	0.07484	0.03777	0.04069	71.79	35.54	-2316	