1

Program: B.Sc.Engg. (IPE) Semster: 3<sup>rd</sup> Semester

Date: 30 September 2022 Time: 2:30 PM-4:00 PM

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

MID SEMESTER EXAMINATION

WINTER SEMESTER: 2021-2022

IPE-4101 Introduction to Industrial & Production Engineering

TIME : 1 HR 30 MIN

FULL MARKS: 75

### There are 3 (Three) questions. Answer all Questions. Marks in the Margin indicate full marks

**01.** (a) Classify the different types of industries and hence specific the different industries based on International Standard Industrial Classifications (ISIC) coding with examples.

(12)

(b) What do you mean by manufacturing systems? Classify and explain the different types manufacturing systems.

(8)

(c) What is Industrial revolution 4.0?

(5)

(CO1), (PO1)

**02.** (a) Explain with necessary diagram the information process cycles involved in a typical manufacturing firm. (15)

(b) Explain the different rules and types of flow pattern that need to be considered for the design of plant layout in industries. (10)

(CO1), (PO1)

**03.** (a) A certain part is routed through six machines in a batch production plant. The setup and operation times for each machine are given in the table below. The batch size is 100 and the average nonoperation time per machine is 12 hours.

Determine: (i) manufacturing lead time and (ii) production rate for operation 3.

Machine	Setup time (hr.)	Operation time (min.)
1	4	5.0
2	2	3.5
3	8	10.0
4	3	1.9
5	3	4.1
6	4	2.5

(b) What do you mean by the term "Utilization" and "Availability"? How the "Utilization" and Availability can be calculated and state its effect on production capacity of a plant? (CO2, CO3), (PO1,PO2)

Program: B. Sc. Engg. (ME/IPE)

Semester: 1st Semester

Date: 5 October, 2022 (Afternoon)

Time: 2:30 am - 4:00 pm

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

**Mid Semester Examination** 

Course Number: Math 4111

Course Title: Modelling with calculus and ODE

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are 3 (three) questions. Answer all questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

Consider the graph of the function f shown in Fig. Q 1(a). Use this graph to 1. a) PO<sub>1</sub> sketch the graphs of the following functions.

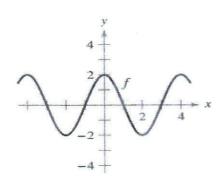


Fig. Q1(a)

(i) 
$$f(x+1)$$
, (ii)  $f(x)+1$ , (iii)  $2f(x)$ , (iv)  $-f(x)$ 

Find a value of the constant k, if possible, that will make the function CO<sub>1</sub> b) PO<sub>1</sub> [10] continuous everywhere.

$$f(x) = \begin{cases} 7x - 2; & x \le 1 \\ kx^2; & x > 1 \end{cases}$$

In the engine shown in Fig. Q 2(a), a 7-inch connecting rod is fastened to 2 a crank of radius 3 inches. The crankshaft rotates counterclockwise at a constant rate of 200 revolutions per minute. Find the velocity of the piston



when  $\theta = \frac{\pi}{3}$ 

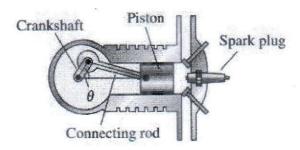


Fig. Q 2(a)

Show that the following function, s(t) satisfies the hypotheses of the Mean-Value theorem over the interval [0, 2], and find all values of c in the interval (0, 2) at which the tangent line to the graph of f is parallel to the secant line joining the points (0, f(0)) and (2, f(2)).

$$s(t) = \frac{1}{4}t^3 + 1$$

Find the absolute extrema of the following function on the indicated closed [10] CO1 interval.

$$g(x) = 2x + 5\cos x$$
; [0,2]

- Sketch a graph of  $y = f(x) = \frac{x^2 1}{x^3}$  and identify the locations of all asymptotes, intercepts, relative extrema, and inflection points. [15] CO1
  - b) Two posts, one 12 feet high and the other 28 feet high, stand 30 feet apart. They are to be stayed by two wires, attached to a single stake, running from ground level to the top of each post. Where should the stake be placed to use the least amount of wire?

The End

Date: 03 Oct. 2022 (afternoon)

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

## DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination Course Number: PHY 4113

Course Title: Structure of Matter, Electricity, Magnetism and

Modern Physics

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are 4 (Four) questions. Answer any 3 (Three) questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

1. (a) What do you understand by quantization and conservation of charges?

(2.5+2.5)

(CO1) (PO1)

(b) Show that the electric field strength E at a distance r from the center of a sphere with a charge q distributed uniformly and of radius R is given by

(10+5)

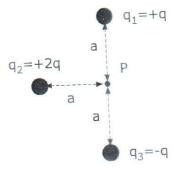
 $E = \left(\frac{q}{4\pi\varepsilon_0 R^3}\right) r$ . Plot the field strength E as a function of r (for r = 0 to r (PO2)

>>R) and explain the points where the value of E will be minimum and maximum.

(c) Consider the charge configuration below. What are the magnitude and direction of the electric field at point P due to this charge configuration?

(05) (CO3)

(PO2)



2. (a) How do you differentiate between electric potential and potential energy?

(05) (CO1)

(15)

(PO1)

(b) Find the expression of electric potential (V) at an arbitrary point P which is at a distance r from the center of an electric dipole.

(CO2) (PO2)

(c) Two-point charges +q and -2q are separated by a distance of 20 m in space. If  $q = 10 \, n$ C, what is the value of electric potential at the midpoint between the charges?

(CO3) (PO2)

(05)

(5)

(15) (CO2)

3. (a) What do you understand by Miller indices? Sketch (201) plane of a cubic crystal.

(CO1) (PO1)

(PO2)

(b) Derive Bragg's law for X-ray diffraction. In Bragg's diffraction condition, can λ be greater than twice of interplanar spacing? Support your answer.



- (c) In a tetragonal crystal, the lattice parameters  $a = b = 2.42 \,\text{Å}$  and  $c = 1.74 \,\text{Å}$ . Determine the interplanar spacing between the consecutive (101) planes. (CO3)
- 4. (a) Classify the crystals on the basis of the nature of the forces acting between the atoms/ions in the crystal. (CO1) (PO1)
  - (b) Obtain an expression for the lattice energy of an ionic crystal in equilibrium. (15) (CO2) (PO2)
  - (c) In a NaCl crystal, the equilibrium distance  $r_0$  between ions is  $0.281 \, nm$  and the binding energy for that crystal is  $7.96 \, eV$ . Calculate the constant n for NaCl. Provided that Madelung constant,  $\alpha = 1.748$  for NaCl crystal. (CO3) (PO2)

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

MID Semester Examination

Course No.: Chem- 4115

Course Title: Physical and Inorganic Chemistry

Winter Semester: A.Y. 2021-2022

Time: 1.0 Hour 30 Minutes

Full Marks: 75

There are **03** (**Three**) Questions. Answer all of them. Marks in the margin indicate full marks. Don't write on this question paper. Symbols carry their usual meanings. Assume reasonable values for any missing data.

Programmable calculators are not allowed.

1.	(a)	Explain Arrhenius and Lewis concepts of acids and bases. Mention the salient features of the concepts with suitable examples.	[06] CO2 PO2
	(b)	What are Ionic Product of water and $p^H$ ? Name two acid base indicators giving structure of Phenolphthalein.	[07] CO2 PO2
	(c)	Describe buffer solution. Give the types and mode of operation of buffer solution.	[012] CO2 PO2
2.	(a)	Define heat of solution and heat of combustion with suitable examples. How can you determine the heat of combustion in a laboratory?	[06] CO3 PO3
	(b)	Define chemical, I potential and Gibb's free energy.	[05] CO3 PO3
	(c)	Calculate $K_p$ for the reaction $N_2$ (g) + $O_2$ (g) $\leftrightarrow$ 2NO (g) at 25°C, when the value of standard free energy ( $\Delta G^{\circ}$ ) is 173 KJ. Comment on the result.	[07] CO3 PO3
	(d)	The heat of reaction of $N_2 + 3H_2 \rightarrow 2NH_3$ at 298K was found to be -21.976 kcal. What will be the heat of reaction at 50°C? The heat capacities Cp at 25°C for $N_2$ , $H_2$ and $NH_3$ are 6.8, 6.77 and 8.86 cal.mol <sup>-1</sup> .deg <sup>-1</sup> respectively.	[07] CO3 PO3
3.	(a)	Derive mathematical equation showing the effect of temperature on the heat of reaction at constant volume and at constant pressure. Name the equation.	[12] CO4 PO2
	(b)	Derive a mathematical equation relating the free energy change ( $\Delta G$ ) and equilibrium constant (K). Mention the significance of the obtained equation.	[13] CO4 PO2



Program: BSc IPE 1st Semester

Semester: Winter

Date: October 04, 2022 (Tuesday)

**Time:** 02:30 pm - 04:00 pm

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

DEPARTMENT OF TECHNICAL AND VOCATIONAL EDUCATION (TVE)

Exam: Mid Semester Examination

Summer Semester: 2021 - 2022

Course Number: Hum 4117

Full Marks: 75

Course Title: Islamic Culture & Professional Ethics

Duration: 90 minutes

### There are 4 (four) questions. Answer 3 (three) questions. Questions 3 and 4 are compulsory. The symbols have their usual meaning.

1.	b)	What is Islam? What differentiates Islam from other religions? The Dalai Lama said: "The purpose of our lives is to be happy". Is this in line with the Islamic view? Support your answers with reference from the Holy Qur'an. Write 5 (five) names among the attributes of Allah with their appropriate meaning.	05 10 10	CO1
2.	b)	List the names of all the children of Prophet Muhammad (PBUH). How many wives did Prophet Muhammad (PBUH) during the course of his life? Mention all their names.  Many of the modern anti-Islamic movements accuse Prophet Muhammad (PBUH) of being a womanizer. How would you defend the personality of our beloved Prophet Muhammad (PBUH) against such claims?	03.5 06.5 15	CO1
3.		Unlike all other religions, Islam is considered as a full package consisting of more than just how to worship the Almighty Allah. Justify this statement? With reference to the Islamic Economic System, prepare elaborate measures that can be used to reduce poverty among the Muslim Ummah.	10 10	CO1
	c)	What is dignity and equality with reference to Human Rights in Islam?	05	CO <sub>2</sub>
4.	a)	Explain the following with reference to Human Rights in Islam:  i. Right to life and safety,  ii. Freedom of belief,  iii. Right to justice.	15	
	b) c)	What does Islam say about the presence of pets (cats, dogs) in our homes?	05 05	CO2



Program: B.Sc. Engg. (IPE)

Semester: 1th Sem.

Date: 28 September 2022

Time: 2:30 pm - 4:00 pm

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination

Course No.: ME 4151

Course Title: Statics and Dynamics

Winter Semester, A. Y. 2021-2022

Time: 1 Hours 30 Min(s)

Full Marks: 75

#### There are 3 (Three) questions. Answer all the questions.

Marks of each question and corresponding CO and PO are written in the brackets. Do not write on this question paper.

- (15)Determine the value of P (as shown in Fig. 1) required to (CO<sub>2</sub>) (i) start the block up the incline, (PO2) (ii) keep it moving up,
  - (iii) prevent it from moving down.

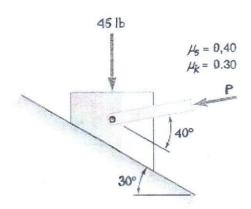


Fig. 1

40 N

390 mm

270 mm

b) Two parallel 40-N forces are applied to a lever as shown in Fig. 2. Determine the moment of the couple formed by the two forces about point A.

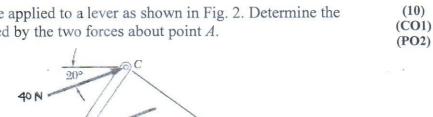


Fig. 2

2. A 10-ft boom is acted upon by a vertical force of 840lb acting on point C as shown in Fig. 3. Determine the tension in each cable T<sub>BD</sub> and T<sub>BE</sub> as well as the reaction at the ball-and-socket joint at A.

(25) (CO1) (PO3)

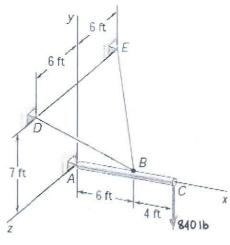


Fig. 3

3. Determine the force in each member of the Pratt bridge truss shown in Fig. 4. State whether each member is in tension or compression.

(25) (CO2) (PO3)

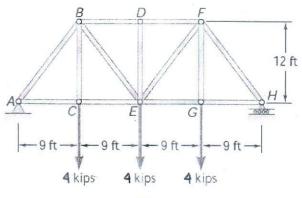


Fig. 4

Program: B.Sc.Engg. (IPE) Semster: 3<sup>rd</sup> Semester Date: 03 October 2022 Time: 10:30 AM-12:00 Noon

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

MID SEMESTER EXAMINATION IPE-4303 Manufacturing Process I

WINTER SEMESTER: 2021-2022 TIME: 1 HR 30 MIN FULL MARKS: 75

#### There are 3 (Three) questions. Answer all Questions. Marks in the Margin indicate full marks

- 01. (a) Explain the fundamentals concept of metal forming processes and hence classify the different metal forming processes with examples. (10)
- (b) Write down the differences between hot working and cold working processes. (8)
- (c) What do you mean by forging process? List some of the common forging processes. (7) (CO1), (PO1)
- 02. (a) Explain with necessary diagram the following rolling processes
  (i) Thread Rolling (ii) Ring Rolling. (12)
- (b) What do you mean by pattern allowance? The casting shown in Figure 1 is to be made in cast iron using a wooden pattern. Assuming only shrinkage allowance as shown in Table below, calculate the dimension of the pattern. All Dimensions are in Inches (13) (CO2), (PO1)

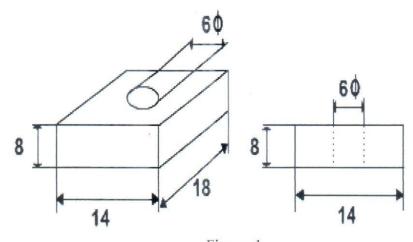


Figure: 1

Table: 1: Shrinkage Allowance

Material	Dimension	Shrinkage allowance (inch/ft)
Grey Cast Iron	Up to 2 2 feet to 4 over 4 feet	feet 0.125 feet 0.105 0.083
Cast Steel	Up to 2 2 feet to 6 over 6 feet	feet 0.251 feet 0.191 0.155
Aluminum	Up to 4 4 feet to 6 over 6 feet	feet 0.155 feet 0.143 0.125

03. (a) Explain with necessary diagram the working principle of Crucible Furnace and Cupola Furnace. (13)

(b) What is sintering? Explain the different heat treatment cycle in sintering process. What will be the design consideration for the fabrication of defect free powder metallurgy product? (12). (CO1, CO2), (PO1)

B.Sc. (ME) / 3<sup>rd</sup> Semester DTE / 1<sup>st</sup> Semester Date: 28<sup>th</sup> September 2022 (Morning)

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination Course Number: ME 4305 Course Title: Basic Thermodynamics Winter Semester: 2021 – 2022 Full Marks: 75

Time: 1.5 Hours

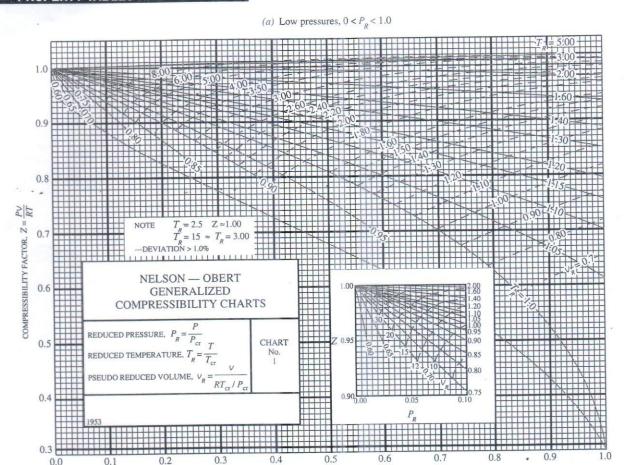
There are **3** (**Three**) questions. Answer **all** the questions. Marks of each question and corresponding COs/POs are written inside the square brackets. The symbols have their usual meanings. Assume any missing data if necessary.

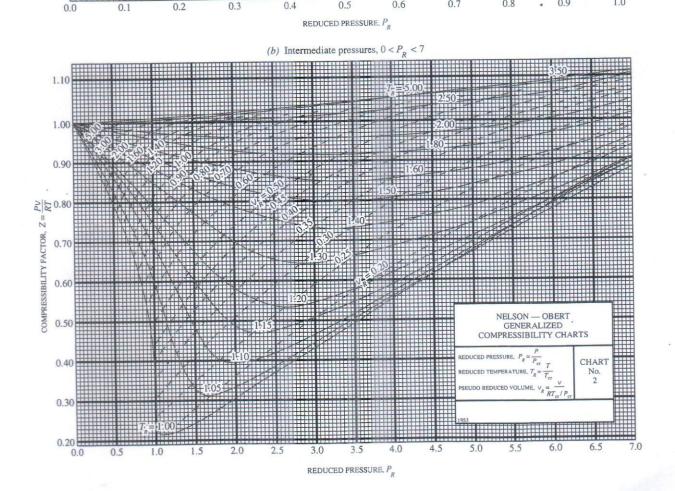
1.	(a) Define the following terms from the context of classical thermodynamics: (i) Principle of corresponding states, (ii) Critical point, (iii) Quality, (iv) The state postulate, (v) Quasi-equilibrium process, (vi) Reference state.	[6] [CO1] [PO1]
	<b>(b)</b> A fixed mass of an ideal gas is heated from 50°C to 80°C at a constant pressure of (i) 1 atm and (ii) 3 atm. In which case do you think the energy required will be greater? Why?	[2] [CO1] [PO2]
	(c) Briefly describe the mechanisms of energy transfer to or from an open system; also, write the energy balance equation for the open system.	[5+1] [CO1] [PO1]
	(d) Is it possible to compress an ideal gas isothermally in an adiabatic piston-cylinder device? Explain.	[2] [CO1] [PO1]
	(e) On a hot summer day, a student turns his fan on when he leaves his room in the morning. When he returns in the evening, will the room be warmer or cooler than the neighboring rooms? Why? Assume all the doors and windows are kept closed.	[1] [CO1] [PO1]
	(f) Define turbine efficiency, generator efficiency, and combined turbine- generator efficiency.	[3] [CO1] [PO1]
	(g) Someone claimed that water vapor could be treated as an ideal gas at all pressures. Do you agree with this claim? Explain your opinion with the necessary figures and examples.	[4] [CO1] [PO1]
	(h) Draw the $T$ - $v$ and $P$ - $T$ diagrams of a pure substance indicating its different regions. Label essential points on the diagrams properly.	[3+3] [CO1] [PO1]
2.	(a) For a saturated liquid-vapor mixture, show that $v_{avg} = v_f + x v_{fg}$ . Symbols carry their usual meanings.	[5] [CO2] [PO2]

(b) An ideal gas undergoes two processes in a piston-cylinder device as [2+5+1-2  $\rightarrow$  Polytropic compression from  $T_1$  and  $P_1$  with a polytropic exponent n[CO2] [PO2] and a compression ratio of  $r = V_1 V_2^{-1}$ . 2-3  $\rightarrow$  Constant pressure expansion at  $P_3 = P_2$  until  $V_3 = V_1$ . i) Sketch the processes on a single *P-V* diagram. ii) Obtain an expression for the ratio of the compression-to-expansion work as a function of n and r. iii) Find the value of this ratio for values of n = 1.4 and r = 6. (c) Show that for a closed system, the boundary work  $W_b$  and the change in [5] internal energy  $\Delta U$  in the first-law relation can be combined into one term, [CO2]  $\Delta H$ , for an isobaric process. [PO2] (d) Large wind turbines with blade span diameters of over 100 m are available [5+1+ for electric power generation. Consider a wind turbine with a blade span 1] diameter of 100 m installed at a site subjected to steady winds at 8 m/s. [CO2] Considering the overall efficiency of the wind turbine to be 32% and the air [PO3] density to be 1.25 kg/m<sup>3</sup>, determine the electric power generated by this wind turbine. Also, assuming steady winds of 8 m/s during a 24-hour period, determine the amount of electric energy and the daily revenue generated for a unit price of \$0.09/kWh for electricity. 3. (a) A 0.016773 m<sup>3</sup> tank contains 1 kg of refrigerant-134a at 110°C. The gas [2+4+constant, critical pressure, and critical temperature of refrigerant-134a are 2] 0.08149 kPa·m<sup>3</sup>/kg·K, 40.59 bar, and 673.56 R, respectively. Determine the [CO2] pressure of the refrigerant using (i) the ideal-gas equation, (ii) the generalized [PO2] compressibility chart, and (iii) the refrigerant tables. (b) A mass of 12 kg of saturated refrigerant-134a vapor is contained in a [12] piston-cylinder device at 240 kPa. Now 300 kJ of heat is transferred to the [CO2] refrigerant at constant pressure while a 110 V source supplies current to a [PO2] resistor within the cylinder for 6 min. Determine the current supplied if the final temperature is 70°C. Also, show the process on a T-v diagram with respect to the saturation lines.

## Figure A-15

922 PROPERTY TABLES AND CHARTS









918
PROPERTY TABLES AND CHARTS

#### TABLE A-12

Saturated refrigerant-134a—Pressure table

		Specific m <sup>3</sup>		Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg·K		
Press., P kPa	Sat. temp., T <sub>sat</sub> °C	Sat. liquid, v <sub>f</sub>	Sat. vapor, v <sub>g</sub>	Sat. liquid, u <sub>f</sub>	Evap., $u_{fg}$	Sat. vapor, $u_g$	Sat. liquid,	Evap.,	Sat. vapor, h <sub>g</sub>	Sat. liquid, $s_f$	Evap.,	Sat. vapor, $s_g$
60	-36.95	0.0007097	0.31108	3.795	205.34	209.13	3.837	223.96	227.80	0.01633	0.94812	0.96445
70	-33.87	0.0007143	0.26921	7.672	203.23	210.90	7.722	222.02	229.74	0.03264	0.92783	0.96047
80	-31.13	0.0007184	0.23749	11.14	201.33	212.48	11.20	220.27	231.47	0.04707	0.91009	0.95716
90	-28.65	0.0007222	0.21261	14.30	199.60	213.90	14.36	218.67	233.04	0.06003	0.89431	0.95434
100	-26.37	0.0007258	0.19255	17.19	198.01	215.21	17.27	217.19	234.46	0.07182	0.88008	0.95191
120	-22.32	0.0007323	0.16216	22.38	195.15	217.53	22.47	214.52	236.99	0.09269	0.85520	0.94789
140	-18.77	0.0007381	0.14020	26.96	192.60	219.56	27.06	212.13	239.19	0.11080	0.83387	0.94467
160	-15.60	0.0007435	0.12355	31.06	190.31	221.37	31.18	209.96	241.14	0.12686	0.81517	0.94202
180	-12.73	0.0007485	0.11049	34.81	188.20	223.01	34.94	207.95	242.90	0.14131	0.79848	0.93979
200	-10.09	0.0007532	0.099951	38.26	186.25	224.51	38.41	206.09	244.50	0.15449	0.78339	0.9378
240	-5.38	0.0007618	0.083983	44.46	182.71	227.17	44.64	202.68	247.32	0.17786	0.75689	0.9347
280	-1.25	0.0007697	0.072434	49.95	179.54	229.49	50.16	199.61	249.77	0.19822	0.73406	0.9322
320	2.46	0.0007771	0.063681	54.90	176.65	231.55	55.14	196.78	251.93	0.21631	0.71395	0.9302
360	5.82	0.0007840	0.056809	59.42	173.99	233.41	59.70	194.15	253.86	0.23265	0.69591	0.9285
400	8.91	0.0007905	0.051266	63.61	171.49	235.10	63.92	191.68	255.61	0.24757	0.67954	0.9271
450	12.46	0.0007983	0.045677	68.44	168.58	237.03	68.80	188.78	257.58	0.26462	0.66093	0.9255
500	15.71	0.0008058	0.041168	72.92	165.86	238.77	73.32	186.04	259.36	0.28021	0.64399	0.9242
550	18.73	0.0008129	0.037452	77.09	163.29	240.38	77.54	183.44	260.98	0.29460	0.62842	0.9230
600	21.55	0.0008198	0.034335	81.01	160.84	241.86	81.50	180.95	262.46	0.30799	0.61398	0.9219
650	24.20	0.0008265	0.031680	84.72	158.51	243.23	85.26	178.56	263.82	0.32052	0.60048	0.9210
700	26.69	0.0008331	0.029392	88.24	156.27	244.51	88.82	176.26	265.08	0.33232	0.58780	0.9201
750	29.06	0.0008395	0.027398	91.59	154.11	245.70	92.22	174.03	266.25	0.34348	0.57582	0.9193
800	31.31	0.0008457	0.025645	94.80	152.02	246.82	95.48	171.86	267.34	0.35408	0.56445	0.9185
850	33.45	0.0008519	0.024091	97.88	150.00	247.88	98.61	169.75	268.36	0.36417	0.55362	0.9177
900	35.51	0.0008580	0.022703	100.84	148.03	248.88	101.62	167.69	269.31	0.37383	. 0.54326	0.9170
950	37.48	0.0008640	0.021456		146.11	249.82	104.52	165.68	270.20	0.38307	0.53333	0.9164
1000	39.37	0.0008700	0.020329	106.47	144.24	250.71	107.34	163.70	271.04	0.39196	0.52378	0.9157
1200	46.29	0.0008935	0.016728	116.72	137.12	253.84	117.79	156.12	273.92	0.42449	0.48870	0.9132
1400	52.40	0.0009167	0.014119	125.96	130.44	256.40	127.25	148.92	276.17	0.45325	0.45742	0.9106
1600	57.88	0.0009400	0.012134		124.05	258.50	135.96	141.96	277.92	0.47921	0.42881	0.9080
1800	62.87	0.0009639	0.010568	142.36	117.85	260.21	144.09	135.14	279.23	0.50304	0.40213	0.9051
2000	67.45	0.0009887	0.009297	149.81	111.75	261.56	151.78	128.36	280.15	0.52519	0.37684	0.9020
2500	77.54	0.0010567	0.006941	167.02	96.47	263.49	169.66	111.18	280.84	0.57542	0.31701	0.8924
3000	86.16	0.0011410	0.005272		80.17	263.26		92.57	279.08	0.62133	0.25759	0.8789





#### 919 APPENDIX 1

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	TABL	E A-13				1					e de la company		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Super	heated ref	rigerant-1	34a									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						ACTOR TO MAKE COMMON TO THE REAL PROPERTY OF							S
Sat. 0.31108 209.13 227.80 0.9645	°C	m³/kg	kJ/kg	kJ/kg	kJ/kg·K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg·K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg·K
-20 0.33608 220.62 240.78 1.0175		$^{*}P = 0.0$	06 MPa (†	$t_{\text{sat}} = -36$	.95°C)	P=0.	10 MPa (7	$r_{\text{sat}} = -26$	.37°C)	P=0.	14 MPa (7	$r_{\text{sat}} = -18$	.77°C)
-10 0.35048 227.57 248.60 1.0478 0.20743 226.77 247.51 1.0031 0.14605 225.93 246.37 0.9724 0.037672 234.67 234.67 256.56 1.0032 0.37893 241.94 264.68 1.1067 0.22506 241.32 263.82 1.0628 0.15908 240.68 262.95 1.0331 0.040705 256.97 281.39 1.1637 0.22506 241.32 263.82 1.0628 0.16544 248.24 271.40 1.0625 0.043495 272.66 298.57 1.1929 0.25937 272.49 298.17 1.1762 0.1812 271.18 1.9719 1.0625 0.043495 272.66 298.57 1.1929 0.25937 272.49 298.17 1.1762 0.1812 271.81 297.59 1.1476 0.044883 280.75 307.68 1.2464 0.26783 280.36 307.15 1.2036 0.19025 279.97 306.61 1.1750 0.44669 289.01 316.77 1.2732 0.7266 288.65 316.28 1.2036 0.19025 279.97 306.61 1.1750 0.04569 289.01 316.77 1.2732 0.7266 288.65 316.28 1.2036 0.19025 279.97 306.61 1.1750 0.04669 289.01 316.77 1.2732 0.7266 288.65 316.28 1.2036 0.19025 279.97 306.61 1.1750 0.05040 314.76 345.01 1.3521 0.30138 314.48 344.61 1.3097 0.20442 296.77 325.11 1.2289 0.49032 306.02 335.43 1.3521 0.30138 314.48 344.61 1.3097 0.21449 314.19 344.22 1.2815 0.1012 0.2504 240.02 262.05 1.0103 0.10955 239.69 261.60 1.0005 0.01240 240.02 245.18 0.9485 0.09991 224.57 244.56 0.9381 0.03434 245.18 0.9485 0.0991 224.57 244.56 0.9381 0.03434 245.18 0.9485 0.0991 224.57 244.56 0.9381 0.03434 245.18 0.9485 0.0991 224.57 244.56 0.9381 0.03434 245.18 0.9485 0.0991 224.57 244.56 0.9381 0.00423 245.06 262.05 1.0103 0.10955 239.69 261.60 1.0005 0.09026 236.61 287.07 1.0718 0.012748 247.66 270.60 1.0400 0.11418 247.36 270.20 1.0304 0.09423 246.76 263.38 1.0134 0.13474 253.33 288.07 1.0976 0.12322 253.09 287.74 1.0822 0.09024 245.80 295.00 1.1257 0.1266 271.16 296.70 1.1164 0.10570 270.73 296.09 1.1002 0.1622 231.39 343.82 1.2003 0.1266 235.10 255.61 0.9271 0.06602 231.39 343.82 1.2003 0.0463 343.94 1.255 0.09024 278.58 306.07 1.1533 0.0266 235.30 2.0566 2.059.99 256.59 0.9366 0.006672 230.34 224.94 24.77 0.9323 0.06382 245.51 265.70 0.9585 0.006642 235.90 235.61 1.2300 0.09024 278.58 306.07 1.1533 0.006669 237.56 258.70 0.9556 0.00644 287.91 286.00 0.07282 296.40 276.70 0.9324 278.58 30.699 250.00 0.06										0.14020	219.56	239.19	0.9447
0 0.36476 234.67 256.56 1.0775 0.21630 233.97 255.60 1.0333 0.15263 233.25 256.61 1.0032 0.03930 249.37 272.95 1.1354 0.23373 248.81 272.18 1.0919 0.16544 248.24 271.40 1.0625 0.0400 2556.97 281.39 1.1637 0.24233 265.45 280.69 1.1204 0.42102 264.73 289.99 1.1916 0.255088 264.27 289.36 1.1455 0.04705 272.66 298.75 1.2192 0.25508 264.27 289.36 1.1455 0.043495 272.66 298.75 1.2192 0.25508 307.15 1.2036 0.043495 272.66 298.75 1.2192 0.25508 307.15 1.0206 0.043485 272.66 298.75 1.2192 0.25508 264.27 289.36 1.1455 0.018412 271.81 297.59 11475 0.046269 289.01 316.77 1.2732 0.27626 288.65 316.28 1.2366 0.19635 288.29 315.78 1.2021 0.0400 2.0400 2.0400 2.0500 2													
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30 0.40705 256.97 281.39 1.1637 0.24233 256.46 280.69 1.1204 0.17172 255.95 279.99 1.0913 40 0.42102 264.73 289.99 1.1916 0.25988 264.27 289.36 1.1485 0.1774 263.80 288.72 1.1196 0.243495 272.66 298.75 1.2192 0.25937 272.24 298.17 1.1762 0.18412 271.81 297.59 1.1475 60 0.44883 280.75 307.68 1.2464 0.26783 280.35 307.15 1.2036 0.19025 279.97 306.61 1.1750 0.46269 289.01 316.77 1.2732 0.7626 288.65 316.28 1.2306 0.19025 279.97 306.61 1.1750 0.46269 289.01 316.77 1.2732 0.7626 288.65 316.28 1.2306 0.19025 279.97 306.61 1.1750 0.40303 306.02 335.43 1.3261 0.29303 305.71 335.01 1.2836 0.20242 296.77 325.11 1.2298 0.47651 297.43 32.602 1.2998 0.28465 297.10 325.57 1.2573 0.20242 296.77 325.11 1.2295 0.50410 314.76 345.01 1.3521 0.30138 314.48 344.61 1.3097 0.21449 314.19 344.22 1.2815 $P = 0.18 \text{ MPa} (T_{set} = -12.73^{\circ}\text{C}) \qquad P = 0.20 \text{ MPa} (T_{set} = -10.09^{\circ}\text{C}) \qquad P = 0.24 \text{ MPa} (T_{set} = -5.38^{\circ}\text{C})   $ Sat. 0.11049 223.01 242.90 0.9398 0.09995 224.51 244.50 0.9379 0.08398 227.17 247.32 0.9348   -10 0.11722 232.49 253.59 0.9799 0.10481 232.11 253.07 0.9699   10 0.12240 240.02 262.05 1.0103 0.10955 239.59 261.60 1.0005 0.09026 239.00 260.66 0.9832   -20 0.12748 247.66 270.60 1.0400 0.1148 247.36 270.20 1.0304 0.09423 246.76 269.38 1.0134													
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60 0.44883 280.75 307.68 1.2464 0.26783 280.36 307.15 1.2036 0.19625 279.97 306.61 1.1750 0.46269 289.01 316.77 1.2732 0.27626 288.65 316.28 1.2306 0.19635 288.29 315.78 1.2021 80 0.47651 297.43 326.02 1.2998 0.28465 297.10 325.57 1.2573 0.20242 296.77 325.11 1.2289 0.49032 306.02 335.43 1.3261 0.29303 305.71 335.01 1.2836 0.20847 305.40 334.59 1.2554 100 0.50410 314.76 345.01 1.3521 0.30138 314.48 344.61 1.3097 0.21449 314.19 344.22 1.2815 24.00 0.1094 223.01 242.90 0.9398 0.09995 224.51 244.50 0.9379 0.08398 227.17 247.32 0.9348 10 0.11722 232.49 253.59 0.9799 0.10481 232.11 253.07 0.9699 0.08617 231.30 251.98 0.9520 0.12748 247.66 270.60 1.0400 0.11418 247.36 270.20 1.0304 0.09423 246.76 269.38 1.0134 0.013741 263.33 288.07 1.0976 0.11824 253.39 297.00 1.1257 0.11874 255.16 278.91 1.0596 0.09812 254.65 278.17 1.0429 0.014715 279.58 306.07 1.1533 0.13206 279.38 305.97 1.1411 0.10942 270.73 296.09 1.1002 0.16622 313.90 343.82 1.2603 0.13641 287.75 316.03 1.1714 0.11310 287.38 315.51 1.2093 0.016622 313.90 343.82 1.2603 0.14933 313.75 343.62 1.2513 0.09994 248.92 249.76 250.85 0.9362 0.016423 229.49 249.77 0.9323 0.14933 313.75 343.62 1.2513 0.12398 313.46 343.22 1.2366 0.0050 0.16622 313.90 343.69 1.2360 0.14933 313.75 343.62 1.2513 0.12398 313.46 343.22 1.2366 0.0050 0.00662 230.39 0.9681 0.06609 237.56 258.70 0.9545 0.05606 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.05609 238.32 256.59 0.9306 0.06609 237.59 248.50 0.05679 252.37 275.09 0.9937 0.00604 227.03 295.95 0.9681 0.00609 237.56 258.70 0.9545 0.05679 252.37 275.09 0.9937 0.006672 262.12 266.40 1.0577 0.07530 261.52 285.72 1.0452 0.00604 287.01 314.01 1.1419 0.08315 285.52 276.66 1.0158 0.05679 252.37 275.09 0.9937 0.006672 262.12 266.40 1.0577 0.07530 261.52 285.72 1.0452 0.06644 287.01 314.01 1.1419 0.08315 285.52 276.66 1.0158 0.06679 252.37 275.09 0.9937 0.00644 287.01 314.01 1.1419 0.08395 286.64 313.50 1.1572 0.06644 287.01 314.01 1.1419 0.08395 286.64 313.50 1.1599 0.06644 287.01 314.01 1.1419 0.08395 286.64 313.50 1.1599 0.066443 285.8													
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$ \begin{array}{c} 80  0.47651  297.43  326.02  1.2998 \\ 90  0.49032  306.02  335.43  1.3261 \\ 100  0.50410  314.76  345.01  1.3521 \\ \hline \\ P = 0.18  \mathrm{MPa}  (T_{\mathrm{sst}} = -12.73^{\circ}\mathrm{C}) \\ \hline \\ P = 0.18  \mathrm{MPa}  (T_{\mathrm{sst}} = -12.73^{\circ}\mathrm{C}) \\ \hline \\ P = 0.20  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.18  \mathrm{MPa}  (T_{\mathrm{sst}} = -12.73^{\circ}\mathrm{C}) \\ \hline \\ P = 0.20  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.20  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -10.09^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ P = 0.24  \mathrm{MPa}  (T_{\mathrm{sst}} = -5.38^{\circ}\mathrm{C}) \\ \hline \\ 0  0.11189  225.04  245.18  0.9485  0.09995  224.51  244.50  0.9379 \\ \hline \\ 10  0.12240  240.02  262.05  1.0103  0.10955  239.69  261.60  1.0005 \\ \hline \\ 0.12240  240.02  262.05  1.0103  0.10955  239.69  261.60  1.0005 \\ \hline \\ 0.12240  240.02  262.05  1.0103  0.11814  247.36  270.20  1.0304 \\ \hline \\ 0.13741  263.33  288.07  1.0996  0.12322  263.09  287.74  1.0882 \\ \hline \\ 0.013741  263.33  288.07  1.0916  0.12322  263.09  287.74  1.0882 \\ \hline \\ 0.014230  271.38  297.00  1.1257  0.12766  271.16  296.70  1.1144 \\ \hline \\ 0.10570  270.73  296.09  1.1026 \\ \hline \\ 0.014715  279.58  306.07  1.1533  0.13206  279.38  305.79  1.141 \\ \hline \\ 0.015196  287.93  315.28  1.1806  0.13641  287.75  315.03  1.174  0.11310  287.38  314.53  1.1269 \\ \hline \\ 0.016149  305.09  334.16  1.2340  0.14504  304.93  333.94  1.2250  0.12338  304.62  333.59  1.226 \\ \hline \\ 0.007642  233.29  294.77  0.9983  0.06368  231.55  $													
$\begin{array}{c} 90  0.49032  306.02  335.43  1.3261 \\ 100  0.50410  314.76  345.01  1.3521 \\ \hline \\ P=0.18  \mathrm{MPa} \left(T_{\mathrm{sst}}=-12.73^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.20  \mathrm{MPa} \left(T_{\mathrm{sst}}=-10.09^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.23  \mathrm{O} \left(T_{\mathrm{sst}}=-10.09^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.25  \mathrm{O} \left(T_{\mathrm{sst}}=-10.09^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.25  \mathrm{O} \left(T_{\mathrm{sst}}=-10.09^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.24  \mathrm{MPa} \left(T_{\mathrm{sst}}=-5.38^{\circ}\mathrm{C}\right) \\ \hline \\ P=0.011722  232.49  253.59  0.9799 \\ \hline \\ 10  0.12240  240.02  262.05  1.0103 \\ \hline \\ 20  0.12748  247.66  270.60  1.0400 \\ \hline \\ 0.13741  263.33  288.07  1.0976 \\ \hline \\ 0.13741  263.33  288.07  1.0976 \\ \hline \\ 0.12322  263.09  287.74  1.0882 \\ \hline \\ 0.014712  270.33  288.07  1.0976 \\ \hline \\ 0.12322  263.09  287.74  1.0882 \\ \hline \\ 0.014715  279.58  306.07  1.1533 \\ \hline \\ 0.015962  231.33  296.43  315.28  1.1806 \\ \hline \\ 0.13641  277.53  315.14  1.0349 \\ \hline \\ 0.01642  305.09  343.82  1.2603 \\ \hline \\ 0.016622  313.90  343.82  1.2603 \\ \hline \\ 0.016622  313.90  343.82  1.2603 \\ \hline \\ 0.007997  246.15  268.54  0.9987 \\ \hline \\ 0.007646  238.29  259.70  0.9681 \\ \hline \\ 0.007646  238.29  259.70  0.9681 \\ \hline \\ 0.007646  238.29  259.70  0.9681 \\ \hline \\ 0.007642  278.88  30.0469  1.1413 \\ \hline \\ 0.008338  248.54  0.0997 \\ \hline \\ 0.009000  270.28  259.48  1.0862 \\ \hline \\ 0.0090000  270.28  259.48  1.0862 \\ \hline \\ 0.00900000000000000000000000000000000$	80												1.2289
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	90	0.49032	306.02	335.43	1.3261								1.2554
Sat.         0.11049         223.01         242.90         0.9398         0.09995         224.51         244.50         0.9379         0.08398         227.17         247.32         0.9348           -10         0.11189         225.04         245.18         0.9485         0.09991         224.57         244.56         0.9381           0         0.1722         232.49         253.59         0.9799         0.10481         232.11         253.07         0.9699         0.08617         231.30         251.98         0.9520           10         0.12740         240.02         262.05         1.0103         0.10955         239.69         261.60         1.0005         0.09026         239.00         260.66         0.9832           20         0.12748         257.43         279.27         1.0691         0.11874         255.16         278.91         1.0596         0.09812         254.63         278.17         1.0429           40         0.13741         263.33         288.07         1.0976         0.12322         263.09         287.74         1.0882         0.10193         262.61         287.07         1.0718           50         0.14715         279.58         306.07         1.1533         0.12366         <	100	0.50410	314.76	345,01	1.3521	0.30138	314.48	344.61	1.3097	0.21449			1.2815
-10 0.11189 225.04 245.18 0.9485 0.09991 224.57 244.56 0.9381 0.011722 232.49 253.59 0.9799 0.10481 232.11 253.07 0.9699 0.08617 231.30 251.98 0.9520 0.10240 240.02 262.05 1.0103 0.10955 239.69 261.60 1.0005 0.09026 239.00 260.66 0.9832 20 0.12748 247.66 270.60 1.0400 0.11418 247.36 270.20 1.0304 0.09423 246.76 269.38 1.0134 30 0.13248 255.43 279.27 1.0691 0.11874 255.16 278.91 1.0596 0.09812 254.63 278.17 1.0429 40 0.13741 263.33 288.07 1.0976 0.12322 263.09 287.74 1.0882 0.10193 262.61 287.07 1.0718 50 0.14230 271.38 297.00 1.1257 0.12766 271.16 296.70 1.1164 0.10570 270.73 296.09 1.1002 0.15196 287.93 315.28 1.1806 0.13641 287.75 315.03 1.1714 0.10942 278.98 305.24 1.1281 0.1596 287.93 315.28 1.1806 0.13641 287.75 315.03 1.1714 0.119042 278.98 305.24 1.1281 0.1596 287.93 315.28 1.1806 0.13641 287.75 315.03 1.1714 0.11910 287.88 314.53 1.1555 80 0.15673 296.43 324.65 1.2075 0.14074 296.27 324.41 1.1984 0.11675 295.93 323.95 1.1826 90 0.16149 305.09 334.16 1.2340 0.14504 304.93 333.94 1.2250 0.12038 304.62 333.51 1.2093 100 0.16622 313.90 343.82 1.2603 0.14933 313.75 343.62 1.2513 0.12398 313.46 343.22 1.2356 0.07282 230.46 250.85 0.9362 10 0.07646 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.051206 235.99 256.59 0.9306 0.09324 278.8 304.69 1.1143 0.0837 256.84 0.9987 0.06925 245.51 267.67 0.9856 0.054213 244.19 265.88 0.9628 30 0.08338 254.08 277.42 1.0285 0.07231 253.52 276.66 1.0158 0.056796 252.37 275.09 0.9937 40 0.08672 262.12 286.40 1.0577 0.07530 261.52 285.72 1.0452 0.05929 260.60 284.32 1.0237 0.09644 287.01 314.01 1.1419 0.08395 286.54 313.50 1.1299 0.066443 285.88 312.45 1.1059 0.0900 270.28 295.48 1.0862 0.07823 259.83 294.87 1.0739 0.061724 268.92 293.61 1.0529 0.008675 295.59 323.48 1.1690 0.08675 295.24 323.00 1.1572 0.06874 294.54 320.04 1.1370 0.0897 322.18 352.69 1.2484 0.09803 321.91 352.31 1.2368 0.075504 321.35 351.55 1.2172 0.00874 333.43 62.72 1.2742 0.09757 331.08 362.36 1.2627 0.07717 330.92 371.89 1.2689 0.10045 340.41 372.55 1.2683 0.079913 339.92 371.89 1.2689 0.10045 340.41		P=0.	18 MPa (	$T_{\rm sat} = -12$	2.73°C)	P=0	.20 MPa (	$T_{\rm sat} = -10$	).09°C)	$P = 0.24 \text{ MPa} (T_{\text{sat}} = -5.38^{\circ}\text{C})$			
-10 0.11189 225.04 245.18 0.9485 0.09991 224.57 244.56 0.9381 0.011722 232.49 253.59 0.9799 0.10481 232.11 253.07 0.9699 0.08617 231.30 251.98 0.9520 10 0.12240 240.02 262.05 1.0103 0.10955 239.59 261.60 1.0005 0.09026 239.00 260.66 0.9832 20 0.12748 247.66 270.60 1.0400 0.11418 247.36 270.20 1.0304 0.09423 246.76 269.38 1.0134 30 0.13248 255.43 279.27 1.0691 0.11874 255.16 278.91 1.0596 0.09812 254.63 278.17 1.0429 40 0.13741 263.33 288.07 1.0976 0.12322 263.09 287.74 1.0882 0.10193 262.61 287.07 1.0718 50 0.14230 271.38 297.00 1.1257 0.12766 271.16 296.70 1.1164 0.10570 270.73 296.09 1.1002 0.13641 287.75 315.03 1.1714 0.10942 278.98 305.24 1.1281 0.1596 287.93 315.28 1.1806 0.13641 287.75 315.03 1.1714 0.10942 278.98 305.24 1.1281 0.015196 287.93 315.28 1.1806 0.13641 287.75 315.03 1.1714 0.11310 287.38 314.53 1.1555 80 0.15673 296.43 324.65 1.2075 0.14074 296.27 324.41 1.1984 0.11675 295.93 323.95 1.1826 0.16149 305.09 334.16 1.2340 0.14504 304.93 333.94 1.2250 0.12038 304.62 333.51 1.2093 100 0.16622 313.90 343.82 1.2603 0.14934 3313.75 343.62 1.2513 0.12398 313.46 343.22 1.2356 0.07282 230.46 250.85 0.9362 10 0.07646 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.051266 235.10 255.61 0.9271 0.00646 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.051266 235.10 255.61 0.9271 0.00644 287.01 314.01 1.1419 0.08395 286.54 313.50 1.1299 0.066443 285.88 312.45 1.0529 0.09302 20.08338 254.08 277.42 1.0285 0.07231 253.52 276.66 1.0158 0.056796 252.37 275.09 0.9937 40 0.08672 262.12 286.40 1.0577 0.07530 261.62 285.72 1.0452 0.05929 260.60 284.32 1.0237 0.09324 278.88 304.69 1.1143 0.08111 278.17 304.12 1.1022 0.066144 277.34 302.98 1.0814 70 0.09644 287.01 314.01 1.1419 0.08395 286.54 313.50 1.1299 0.066443 285.88 312.45 1.1095 0.08675 295.59 323.48 1.1690 0.08675 295.24 323.00 1.1572 0.06874 294.54 320.04 1.1370 0.0875 313.17 342.81 1.2223 0.09229 312.87 342.41 1.2106 0.073274 312.28 341.59 1.1908 0.08675 295.24 323.00 1.1572 0.06874 294.54 320.04 1.1370 0.0897 322.18 352.69 1.2484 0.09503 321.91 352.31 1	Sat.	0.11049	223.01	242.90	0.9398	0.09995	224.51	244.50	0.9379	0.08398	227.17	247.32	0.9348
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-10	0.11189				0.09991							
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0	0.11722	232.49			0.10481	232.11	253.07	0.9699	0.08617	231,30	251.98	0.9520
30 0.13248 255.43 279.27 1.0691						0.10955	239.69	261.60	1.0005	0.09026	239.00	260.66	0.9832
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80 0.15673 296.43 324.65 1.2075 0.14074 296.27 324.41 1.1984 0.11675 295.93 323.95 1.1826 90 0.16149 305.09 334.16 1.2340 0.14504 304.93 333.94 1.2250 0.12038 304.62 333.51 1.2093 0.14933 313.75 343.62 1.2513 0.12398 313.46 343.22 1.2356 $P = 0.28  \text{MPa}  (T_{\text{sat}} = -1.25^{\circ}\text{C})$ $P = 0.32  \text{MPa}  (T_{\text{sat}} = 2.46^{\circ}\text{C})$ $P = 0.40  \text{MPa}  (T_{\text{sat}} = 8.91^{\circ}\text{C})$ Sat. 0.07243 229.49 249.77 0.9323 0.06368 231.55 251.93 0.9303 0.051266 235.10 255.61 0.9271 0.07282 230.46 250.85 0.9362 10 0.07646 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.051506 235.99 256.59 0.9306 0.07997 246.15 268.54 0.9987 0.06925 245.51 267.67 0.9856 0.054213 244.19 265.88 0.9628 30 0.08338 254.08 277.42 1.0285 0.07231 253.52 276.66 1.0158 0.056796 252.37 275.09 0.9937 40 0.08672 262.12 286.40 1.0577 0.07530 261.52 285.72 1.0452 0.059292 260.60 284.32 1.0237 50 0.09000 270.28 295.48 1.0862 0.07823 269.83 294.87 1.0739 0.061724 268.92 293.61 1.0529 0.09324 278.58 304.69 1.1143 0.08111 278.17 304.12 1.1022 0.064104 277.34 302.98 1.0814 70 0.09644 287.01 314.01 1.1419 0.08395 286.54 313.50 1.1299 0.066443 285.88 312.45 1.1095 80 0.09961 295.59 323.48 1.1690 0.08675 295.24 323.00 1.1572 0.068747 294.54 322.04 1.1370 90 0.10275 304.30 333.07 1.1958 0.08953 303.99 332.64 1.1841 0.071023 303.34 331.75 1.1641 1.0 0.10897 322.18 352.69 1.2484 0.09503 321.91 352.31 1.2368 0.079513 339.92 371.89 1.2689 1.2689 1.2098 1.2008													
90 0.16149 305.09 334.16 1.2340 0.14504 304.93 333.94 1.2250 0.12038 304.62 333.51 1.2093 0.14933 313.75 343.62 1.2513 0.12398 313.46 343.22 1.2356 $P = 0.28 \text{ MPa} (T_{\text{sat}} = -1.25^{\circ}\text{C})$ $P = 0.32 \text{ MPa} (T_{\text{sat}} = 2.46^{\circ}\text{C})$ $P = 0.40 \text{ MPa} (T_{\text{sat}} = 8.91^{\circ}\text{C})$ Sat. 0.07243 229.49 249.77 0.9323 0.06368 231.55 251.93 0.9303 0.051266 235.10 255.61 0.9271 0.07646 238.29 259.70 0.9681 0.06609 237.56 258.70 0.9545 0.051506 235.99 256.59 0.9306 0.07997 246.15 268.54 0.9987 0.06925 245.51 267.67 0.9856 0.054213 244.19 265.88 0.9628 30 0.08338 254.08 277.42 1.0285 0.07231 253.52 276.66 1.0158 0.056796 252.37 275.09 0.9937 40 0.08672 262.12 286.40 1.0577 0.07530 261.62 285.72 1.0452 0.059292 260.60 284.32 1.0237 50 0.09000 270.28 295.48 1.0862 0.07823 269.83 294.87 1.0739 0.061724 268.92 293.61 1.0529 60 0.09324 278.58 304.69 1.1143 0.08111 278.17 304.12 1.1022 0.064104 277.34 302.98 1.0814 70 0.09644 287.01 314.01 1.1419 0.08395 286.64 313.50 1.1299 0.066443 285.88 312.45 1.1095 80 0.09961 295.59 323.48 1.1690 0.08675 295.24 323.00 1.1572 0.068747 294.54 322.04 1.1370 0.010587 313.17 342.81 1.2223 0.09229 312.87 342.41 1.2106 0.073274 312.28 341.59 1.1908 10 0.10587 313.17 342.81 1.2223 0.09229 312.87 342.41 1.2106 0.073274 312.28 341.59 1.1908 10 0.10687 322.18 352.69 1.2484 0.099503 321.91 352.31 1.2368 0.075504 321.35 351.55 1.2172 120 0.11205 331.34 362.72 1.2742 0.09775 331.08 362.36 1.2627 0.077717 330.56 361.65 1.2432 130 0.11512 340.65 372.88 1.2998 0.10045 340.41 372.55 1.2883 0.079913 339.92 371.89 1.2689													
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$P = 0.28 \text{ MPa } (T_{\text{sat}} = -1.25^{\circ}\text{C}) \qquad P = 0.32 \text{ MPa } (T_{\text{sat}} = 2.46^{\circ}\text{C}) \qquad P = 0.40 \text{ MPa } (T_{\text{sat}} = 8.91^{\circ}\text{C})$ Sat. $0.07243$ $229.49$ $249.77$ $0.9323$ $0.06368$ $231.55$ $251.93$ $0.9303$ $0.051266$ $235.10$ $255.61$ $0.9271$ $0.07282$ $230.46$ $250.85$ $0.9362$ $10$ $0.07646$ $238.29$ $259.70$ $0.9681$ $0.06609$ $237.56$ $258.70$ $0.9545$ $0.051506$ $235.99$ $256.59$ $0.9306$ $20$ $0.07997$ $246.15$ $268.54$ $0.9987$ $0.06925$ $245.51$ $267.67$ $0.9856$ $0.054213$ $244.19$ $265.88$ $0.9628$ $30$ $0.08338$ $254.08$ $277.42$ $1.0285$ $0.07231$ $253.52$ $276.66$ $1.0158$ $0.056796$ $252.37$ $275.09$ $0.9937$ $40$ $0.08672$ $262.12$ $286.40$ $1.0577$ $0.07530$ $261.62$ $285.72$ $1.0452$ $0.059292$ $260.60$ $284.32$ $1.0237$ $260$ $0.09324$ $278.58$ $304.69$ $1.1143$ $0.08111$ $278.17$ $304.12$ $1.1022$ $0.064104$ $277.34$ $302.98$ $1.0814$ $270$ $2$													
Sat.         0.07243         229.49         249.77         0.9323         0.06368         231.55         251.93         0.9303         0.051266         235.10         255.61         0.9271           0         0.07282         230.46         250.85         0.9362         0.06609         237.56         258.70         0.9545         0.051506         235.99         256.59         0.9306           20         0.07997         246.15         268.54         0.9987         0.06925         245.51         267.67         0.9856         0.054213         244.19         265.88         0.9628           30         0.08338         254.08         277.42         1.0285         0.07231         253.52         276.66         1.0158         0.056796         252.37         275.09         0.9937           40         0.08672         262.12         286.40         1.0577         0.07530         261.62         285.72         1.0452         0.059292         260.60         284.32         1.0237           50         0.09000         270.28         295.48         1.0862         0.07823         269.83         294.87         1.0739         0.061724         268.92         293.61         1.0529           60         0.09324	100	0.10022	313.90	343.02	1.2003	0.14933	313./5	343.02	1,2313	0.12398	313.40	343,22	1.2356
0       0.07282       230.46       250.85       0.9362         10       0.07646       238.29       259.70       0.9681       0.06609       237.56       258.70       0.9545       0.051506       235.99       256.59       0.9306         20       0.07997       246.15       268.54       0.9987       0.06925       245.51       267.67       0.9856       0.054213       244.19       265.88       0.9628         30       0.08338       254.08       277.42       1.0285       0.07231       253.52       276.66       1.0158       0.056796       252.37       275.09       0.9937         40       0.08672       262.12       286.40       1.0577       0.07530       261.62       285.72       1.0452       0.059292       260.60       284.32       1.0237         50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       <		Andrew Management			Marie Note Street and Street	BOOK STREET, S		The state of the s		Carried Street, March Street,			SEPREMENTAL ALCOHOLOGICAL
10       0.07646       238.29       259.70       0.9681       0.06609       237.56       258.70       0.9545       0.051506       235.99       256.59       0.9306         20       0.07997       246.15       268.54       0.9987       0.06925       245.51       267.67       0.9856       0.054213       244.19       265.88       0.9628         30       0.08338       254.08       277.42       1.0285       0.07231       253.52       276.66       1.0158       0.056796       252.37       275.09       0.9937         40       0.08672       262.12       286.40       1.0577       0.07530       261.62       285.72       1.0452       0.059292       260.60       284.32       1.0237         50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08875       295.24       323.00       1.1572						0.06368	231.55	251.93	0.9303	0.051266	235.10	255.61	0.9271
20       0.07997       246.15       268.54       0.9987       0.06925       245.51       267.67       0.9856       0.054213       244.19       265.88       0.9628         30       0.08338       254.08       277.42       1.0285       0.07231       253.52       276.66       1.0158       0.056796       252.37       275.09       0.9937         40       0.08672       262.12       286.40       1.0577       0.07530       261.62       285.72       1.0452       0.059292       260.60       284.32       1.0237         50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1,1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572						0.06600	227.56	259.70	0.0545	0.051506	225.00	250 50	0.0200
30       0.08338       254.08       277.42       1.0285       0.07231       253.52       276.66       1.0158       0.056796       252.37       275.09       0.9937         40       0.08672       262.12       286.40       1.0577       0.07530       261.62       285.72       1.0452       0.059292       260.60       284.32       1.0237         50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1,1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841				STATE OF THE PARTY OF THE PARTY.									
40       0.08672       262.12       286.40       1.0577       0.07530       261.62       285.72       1.0452       0.059292       260.60       284.32       1.0237         50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1,1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>The second secon</td> <td>A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY.</td> <td></td> <td></td> <td></td>									The second secon	A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY.			
50       0.09000       270.28       295.48       1.0862       0.07823       269.83       294.87       1.0739       0.061724       268.92       293.61       1.0529         60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1,1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106       0.073274       312.28       341.59       1.1908         110       0.10897       322.18       352.69       1.2484       0.09503       321.91       352.31       1.2368 <td>CATALON CONTRACTOR</td> <td></td>	CATALON CONTRACTOR												
60       0.09324       278.58       304.69       1.1143       0.08111       278.17       304.12       1.1022       0.064104       277.34       302.98       1.0814         70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1,1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106       0.073274       312.28       341.59       1.1908         110       0.10897       322.18       352.69       1.2484       0.09503       321.91       352.31       1.2368       0.075504       321.35       351.55       1.2172         120       0.11205       331.34       362.72       1.2742       0.09775       331.08       362.36       1.2627 </td <td></td>													
70       0.09644       287.01       314.01       1.1419       0.08395       286.64       313.50       1.1299       0.066443       285.88       312.45       1.1095         80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106       0.073274       312.28       341.59       1.1908         110       0.10897       322.18       352.69       1.2484       0.09503       321.91       352.31       1.2368       0.075504       321.35       351.55       1.2172         120       0.11205       331.34       362.72       1.2742       0.09775       331.08       362.36       1.2627       0.077717       330.56       361.65       1.2432         130       0.11512       340.65       372.88       1.2998       0.10045       340.41       372.55       1.2883<						Control Control of the State of							
80       0.09961       295.59       323.48       1.1690       0.08675       295.24       323.00       1.1572       0.068747       294.54       322.04       1.1370         90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106       0.073274       312.28       341.59       1.1908         110       0.10897       322.18       352.69       1.2484       0.09503       321.91       352.31       1.2368       0.075504       321.35       351.55       1.2172         120       0.11205       331.34       362.72       1.2742       0.09775       331.08       362.36       1.2627       0.077717       330.56       361.65       1.2432         130       0.11512       340.65       372.88       1.2998       0.10045       340.41       372.55       1.2883       0.079913       339.92       371.89       1.2689					SPECIAL PROPERTY AND PARTY OF THE	THE RESERVE OF THE PERSON HERE							
90       0.10275       304.30       333.07       1.1958       0.08953       303.99       332.64       1.1841       0.071023       303.34       331.75       1.1641         100       0.10587       313.17       342.81       1.2223       0.09229       312.87       342.41       1.2106       0.073274       312.28       341.59       1.1908         110       0.10897       322.18       352.69       1.2484       0.09503       321.91       352.31       1.2368       0.075504       321.35       351.55       1.2172         120       0.11205       331.34       362.72       1.2742       0.09775       331.08       362.36       1.2627       0.077717       330.56       361.65       1.2432         130       0.11512       340.65       372.88       1.2998       0.10045       340.41       372.55       1.2883       0.079913       339.92       371.89       1.2689						The state of the s	COLUMN TO THE PARTY OF THE PART			CHARLES AND APPROXIMATION TO THE PARTY OF TH	A STREET OF BOOK IS ASSAULT OF		
100     0.10587     313.17     342.81     1.2223     0.09229     312.87     342.41     1.2106     0.073274     312.28     341.59     1.1908       110     0.10897     322.18     352.69     1.2484     0.09503     321.91     352.31     1.2368     0.075504     321.35     351.55     1.2172       120     0.11205     331.34     362.72     1.2742     0.09775     331.08     362.36     1.2627     0.077717     330.56     361.65     1.2432       130     0.11512     340.65     372.88     1.2998     0.10045     340.41     372.55     1.2883     0.079913     339.92     371.89     1.2689						and the second s				The state of the s			
110     0.10897     322.18     352.69     1.2484     0.09503     321.91     352.31     1.2368     0.075504     321.35     351.55     1.2172       120     0.11205     331.34     362.72     1.2742     0.09775     331.08     362.36     1.2627     0.077717     330.56     361.65     1.2432       130     0.11512     340.65     372.88     1.2998     0.10045     340.41     372.55     1.2883     0.079913     339.92     371.89     1.2689						THE COURSE OF STREET STREET, S		342.41	1.2106	A STATE OF THE PARTY OF THE PAR			
120     0.11205     331.34     362.72     1.2742     0.09775     331.08     362.36     1.2627     0.077717     330.56     361.65     1.2432       130     0.11512     340.65     372.88     1.2998     0.10045     340.41     372.55     1.2883     0.079913     339.92     371.89     1.2689	110	0.10897	322.18	352.69	1.2484								
						0.09775		362.36	1.2627	0.077717	330.56		1.2432
140 0 11818 350 11 383 20 1 3251 1 0 10314 349 88 382 80 1 3136 1 0 082006 340 42 302 36 1 2042						A STATE OF THE PARTY OF THE PAR							1.2689
243 0.11010 330.11 303.20 1.3231 1 0.10314 343.00 302.03 1.3130 1 0.002030 343.42 382.20 1.2943	140	0.11818	350.11	383.20	1.3251	0.10314	349.88	382.89	1.3136	0.082096	349.42	382.26	1.2943





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PROPERTY TABLES AND CHARTS

	LE A-13	Max was									A Company	
CONTRACTOR STORY	rheated refr					A Desired Police				Name of particles	1 - 0.0	
T °C	v m³/kg	u kJ/kg	h kJ/kg	s kJ/kg·K	m <sup>3</sup> /kg	u kJ/kg	h kJ/kg	s kJ/kg·K	m <sup>3</sup> /kg	u kJ/kg	h kJ/kg	s kJ/kg·K
	P = 0.1	50 MPa (7	$r_{sat} = 15.7$	'1°C)	P=0.	60 MPa (	$T_{\rm sat} = 21.$	55°C)	P=0.	70 MPa (7	$r_{\rm sat} = 26.6$	59°C)
Sat.	0.041168	238.77	259.36	0.9242	0.034335				0.029392	THE RESERVE OF THE PARTY OF THE		
20	0.042115	242.42	263.48									
30	0.044338	250.86	273.03		0.035984		270.83	0.9500	0.029966	247.49		0.9314
40	0.046456	259.27	282.50		0.037865			0.9817	0.031696			0.9642
50	0.048499	267.73	291.98		0.039659		290.30	1.0122	0.033322			
60	0.050485	276.27			0.041389			1.0417	0.034875			1.0257
70	0.052427	1000 PER		1.0884	0.043069			1.0706	0.036373			1.0550
80	0.054331	293.65	320.82		0.044710			1.0988	0.037829			1.0835
100	0.056205	311.52	330.63 340.55		0.046318			1.1265	0.039250			1.1115
110	0.059880	320.65	350.59		0.047900			1.1336	0.040642			1.1659
120	0.061687	329.91			0.050997			1.2068	SALE PRODUCTION OF THE PROPERTY OF THE PARTY	328.57		1.1925
130	0.063479	339.31		1.2492	0.052519			1.2328	0.044688			
140	0.065256	348.85		1.2747	0.054027			1.2585	0.046004			1.2445
150	0.067021	358.52	392.04		0.055522		391.29	1.2838	0.047306			
160	0.068775	368.34			0.057006			1.3089	0.048597			
	P=0.	80 MPa (7	$T_{\rm sat} = 31.3$	31°C)	P=0	.90 MPa	$(T_{\text{sat}} = 35)$	.51°C)	P = 1.	00 MPa (7	$T_{\rm sat} = 39.3$	37°C)
Sat.	0.025645	246.82	267.34	0.9185	0.022686	248.82	269.25	0.9169	0.020319	250.71	271.04	0.9157
40	0.027035	254.84		0.9481		253.15		0.9328	0.020406	251.32	271.73	0.9180
50	0.028547		THE PERSON NAMED IN	0.9803	0.024809				0.021796	260.96	282.76	0.9526
60		272.85		1.0111	0.026146				0.023068		293.40	
70	0.031340			1.0409	0.027413			1.0280	0.024261			
80	0.032659			1.0699	0.028630				0.025398		314.27	
90	0.033941	299.97		1.0982	0.029806			1.0861	0.026492			
100	0.035193	309.17		1.1259	0.030951	308.35	336.21	1.1141	0.027552		335.08	
120	0.030420	318.47 327.89		1.1798	0.032068 0.033164			1.1415	0.028584 0.029592		356.08	
130	0.037623	337.42		1.2062	0.033104				0.029592		366.70	
140	0.039985				0.035302				0.030581			
150	0.041143			1.2577	0.036349			1.2468	0.032512		388.24	
160	0.042290	366.78		1.2830	0.037384			1.2722	0.033457			1.2624
170	0.043427	376.83	411.57		0.038408	376.33	410.89	1.2973	0.034392	375.82	410.22	
180	0.044554		422.65	1.3328	0.039423	386.54	422.02	1.3221	0.035317	386.06		
	P=1.	20 MPa (1	$T_{\rm sat} = 46.2$	29°C)	P=1	.40 MPa	$(T_{\rm sat} = 52)$	.40°C)	P = 1.	60 MPa (	$T_{\rm sat} = 57.8$	38°C)
	0.016728				0.014119	256.40	276.17	0.9107	0.012134	258.50	277.92	0.9080
	0.017201				0.015005	0011	005.4-	0.0000	00000	000.01	000.74	0.0161
60	0.018404		289.66		0.015005				0.012372		280.71	
	0.019502		300.63		0.016060				0.013430		293.27	
80	0.020529 0.021506			1.0249	0.017023				0.014362 0.015215		305.09	
	0.021300	305.81		1.0836	0.017923				0.015215		327.78	
	0.022442		343.41		0.019778				0.016014			
	0.024228	325.05		1.1395	0.020388				0.0177500			
THE BUTHARD PROPERTY	0.025086	334.79		1.1665	0.021155				0.018201			
	0.025927			1.1931	0.021904				0.018882			
	0.026753	354.57		1.2192	0.022636				0.019545			
160	0.027566	364.63		1.2450	0.023355				0.020194		394.71	
170	0.028367		408.84		0.024061				0.020830			
180	0.029158	385.10	420.09	1.2955	0.024757	384.12	418.78	1.2808	0.021456			
AND PARTY.		Service de 40	PART OF STREET			A CONTRACTOR			SERVE SERVE	214		1 AL 35

19

Program: B. Sc. Engg. (ME/IPE/BSc TE)

Semester: 3<sup>rd</sup>/2 Y 1<sup>st</sup> Semester

Date: 5 October, 2022

Time: 10:30 am - 12:00 noon

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination Course Number: math 4311/4599

Course Number: math 4311/4599 Course Title: Vector Analysis, Multivariable Calculus

and Complex Variables

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are 3 (three) questions. Answer all of them. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

- (a) Examine whether the vectors i-2j+3k, 5i+6j-k and 3i+2j+k [11] form a linearly dependent set or a linearly independent set. If dependent, find a linear relation among them.
  - (b) Find the area of the parallelogram having diagonals 3i + j 2k and [07] i 3j + 4k. [CO1, PO1]
  - (c) Give the geometrical interpretation of the cross product of vectors. [07]
    [CO1,
    PO1]
- (a) Find the volume of the parallelepiped whose edges are represented by the vectors c × a, a × b and b × c.
  [CO1, PO1]
  - (b) If  $\mathbf{F}(x, y, z) = x^2 yz \mathbf{i} 2xz^3 \mathbf{j} + xz^2 \mathbf{k}$  and  $\mathbf{G}(x, y, z) = 2z \mathbf{i} + y \mathbf{j} + x^2 \mathbf{k}$ , [13] [CO1, poly find  $\frac{\partial^2}{\partial x \partial y} (\mathbf{F} \times \mathbf{G})$  at (1, 0, -2).
- 3. (a) Find the directional derivative of  $\phi(x, y, z) = 4xz^3 3x^2y^2z$  at (2, -1, 2) in the direction of the vector  $2\mathbf{i} 3\mathbf{j} + 6\mathbf{k}$ .
  - (b) Find an equation for the tangent plane to the surface  $2xz^2 3xy 4x = 7$  [12] at the point (3, -1, 2). [CO1, PO1]



1

Name of the Program: B.Sc. ME

Semester: Winter semester

Date: October 04, 2022 (Tuesday)

**Time:** 10:30 am- 12:00 pm

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC) DEPARTMENT OF TECHNICAL AND VOCATIONAL EDUCATION (TVE)

Exam: Mid Semester Examination

Summer Semester: 2021 - 2022

Course Number: Hum 4317

Full Marks: 75

Course Title: Science Technology and Islam

**Duration:** 90 minutes

#### There are 4 (four) questions. Answer any 3 (three) questions

1.	a) b)	What is Big-Bang Theory? Mention the Quranic evidence about this theory. Describe the view of the Quran about the expansion of the Universe with the scientific opinion.  What is your understanding about Big-Crunch? What is the view of the Holy	10 10	CO1, CO2	PO9/ PO10
	-)	Quran about Big-Crunch? Discuss.	05		
2.	a)	Discuss the Fine-tuning and perfect balance of the universe and mention the verse of the Quran in this regard.	10	CO1,	
	b)	Describe the creation and formation of the earth.	10		PO10
	c)	Discuss about the "Unique rotation of the Universe".	05		
3.	a)	Describe the fundamental force in physics with the references from the Holy Ouran.	10	CO1,	
	b)	"Everything created in pairs"-Explain the statement with reference from the Holy Quran and scientific opinion.	10	CO5	PO6/ PO7
	c)		05		
4.	a)	는 어린 사람이 있는 경기를 보고 있다면 보면 되었다. 그는 사람이 되었는데 보면 되었다면 보면 되었다면 보면 되었다면 보면 되었다면 보면 되었다면 보면 되었다면 되었다면 되었다면 되었다면 되었다면 보면 보다는데 보면 되었다면 보면	10	CO1,	
	b)	Holy Quran with scientific view.	10	CO2, CO5	PO6/ PO7
	()	Describe about the entoryo development in the Hory Quian.	05		

Program: BSc. Eng.(ME) / DTE (1<sup>St</sup> sem) Semester: 3<sup>rd</sup>, Winter

Date: 3 October 2022 Time: 10:30 am to 12:00 pm

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid-Semester Examination

Winter Semester, A.Y. 2021-2022

Course No. ME 4325

Time

: 1½ hours

Course Title: Material Engineering

Full Marks

: 75

There are 4 (Four) Questions. Answers to questions 1 and 4 are compulsory. Answer either question 2 or 3. Answer 3 (Three) questions altogether. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

qu	estio	n and corresponding CO and PO are written in the brackets.	
1	a)	Two materials can have similar toughness with different stiffness values. From stress-strain curves for such cases choose one for a design where high plastic deformation is preferred. Again, different methods are used to measure the stiffness of different metals and alloys. List the methods used to estimate stiffness from the stress-strain curves where the yield point may or may not be sharp.	12.5 (CO1) (PO1, PO2)
	b)	The same material can be either ductile or brittle based on its operating temperature. With necessary sketches describe how deformation types can be identified from fracture surfaces. Explain how operating temperature controls the mode of fracture.	12.5 (CO2) (PO2, PO3)
2		Sketch the unit cells of SC, BCC, and FCC crystal structures. Calculate packing density for all these three crystal structures and show that FCC can be categorized as the most packed lattice type among all. Also, build a BCC structure from two interpenetrating SC with a neat sketch and explain when to be considered as SC and when as BCC.	25 (CO1, CO2) (PO1, PO2,
3		Q3 is an alternative to Q2 (answer either one) Using neat sketches calculate the number of atoms per unit cell of SC, BCC, and FCC crystal structures. Also, calculate the number of nearest neighbor and next nearest neighbor for these crystal structures with the relevant distances. Comment on how these factors play a role to build materials' ductile properties.	PO3)
4	a)	Distinguish between crystal structure and lattice. Using neat sketches, explain how symmetry limits the total number of crystal structures in 2-D to four and total number of lattice types to five.	12.5 (CO1) (PO1, PO2)
	b)	Distinguish between creep and fatigue failure. Discuss fatigue life and fatigue limit. Explain how a dynamic loading system leads to failure at a much lowers strength than the yield strength of a material.	12.5 (CO1) (PO1, PO2)



Program: B. Sc. in IPE Semester: Winter semester Date: 28 September, 2022 Time: 10:30 am - 12:00 pm

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination

Winter Semester: 2021 - 2022

Course Number: ME 4353

Full Marks: 75 Time: 1.5 Hours

Course Title: Thermodynamics and Heat Transfer

There are **3** (three) questions. Answer all **3** (three) questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

(Property tables are attached at page -3)

optimize the piston clearance?

1. a) i) Distinguish between the SIE and CIE combustion processes with the help of a neat sketch.

ii) Define piston clearance. Why is it so crucial for an engine? How can you (PO1/PO2)

b) Consider the following specifications for a square engine.

(CO2)

(10)

(CO2)

(PO1/PO2)

Configuration: V10	Volume: 4000 cc
Engine speed: 2500 rpm	Cut-off ratio: 1.8
Brake torque: 11.5 Nm	Total clearance volume: 0.2 L
Length of connecting rod: 350 i	nm
Fuel consumption rate: 2.22 x 1	0 <sup>-4</sup> kg/s

#### Calculate:

- i. Connecting rod to crank radius ratio.
- ii. The air standard efficiency (%) of the engine. (k = 1.4)
- iii. The brake power (kW) at the flywheel.
- iv. The brake specific fuel consumption rate (g/kW-h)
- 2. a) Differentiate between a 4-stroke and 2-sroke engine in terms of Power-to-weight ratio. Also, describe why the 2-stroke engine is getting phased out now-a-days.

  (CO2)

  (PO1/PO2)
  - b) Compute the higher heating value of 'octane' when the lower heating value (9) is 44.4 MJ/kg. (CO2)

(PO1/PO2)

- 3. a) Distinguish between a 'control mass' system and a 'control volume' system with necessary examples. On which condition a 'control mass' system can be approximated as an 'isolated system'? (CO1)

  (PO1/PO2)
  - b) "Work is a path function"- Explain. (4)
    (CO1)
    (PO1/PO2)
  - c) During the combustion of gasoline in a SIE, 200 kW heat is produced which is completely converted into work by the wheels. Does this scenario violate the 2<sup>nd</sup> law of thermodynamics? Explain in terms of Kelvin-Plank Statement. (PO1/PO2)
  - d) A mass of 15 kg of air in a piston-cylinder device is heated from 29°C to 77°C by passing current of 5A through a resistance heater inside the cylinder (as shown in Fig. 1). The pressure inside the cylinder is held constant at 300 kPa during the process, and a heat loss of 60 kJ occurs. Determine the voltage of the resistance heater.

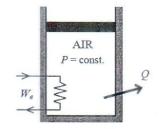


Fig. 1 A piston-cylinder device

TABLE A-2
Ideal-gas specific heats of various common gases (Continued)

(b) At various	temperature	5								
Temperature,	$c_p$ kJ/kg·K	c <sub>v</sub> kJ/kg⋅K	k	c <sub>p</sub> kJ/kg⋅K	c, kJ/kg⋅K	k	c <sub>p</sub> kJ/kg⋅K	c, kJ/kg⋅K	k	
K		Air		Car	Carbon dioxide, CO <sub>2</sub>			Carbon monoxide, CO		
250	1.003	0.716	1.401	0.791	0.602	1.314	1.039	0.743	1.400	
300	1.005	0.718	1.400	0.846	0.657	1.288	1.040	0.744	1.399	
350	1.008	0.721	1.398	0.895	0.706	1.268	1.043	0.746	1.398	
400	1.013	0.726	1.395	0.939	0.750	1.252	1.047	0.751	1.395	
450	1.020	0.733	1.391	0.978	0.790	1.239	1.054	0.757	1.392	
500	1.029	0.742	1.387	1.014	0.825	1.229	1.063	0.767	1.387	
550	1.040	0.753	1.381	1.046	0.857	1.220	1.075	0.778	1.382	
600	1.051	0.764	1.376	1.075	0.886	1.213	1.087	0.790	1.376	
650	1.063	0.776	1.370	1.102	0.913	1.207	1.100	0.803	1.370	
700	1.075	0.788	1.364	1.126	0.937	1.202	1.113	0.816	1.364	
750	1.087	0.800	1.359	1.148	0.959	1.197	1.126	0.829	1.358	
800	1.099	0.812	1.354	1.169	0.980	1.193	1.139	0.842	1.353	
900	1.121	0.834	1.344	1.204	1.015	1.186	1.163	0.866	1.343	
1000	1.142	0.855	1.336	1.234	1.045	1.181	1.185	0.888	1.335	

TA	DI	E	A	17
18	DL	·E	House	11

T	h		U		s°		
K	kJ/kg	$P_r$	kJ/kg	$V_r$	kJ/kg·K		
200	199.97	0.3363	142.56	1707.0	1.29559		
210	209.97	0.3987	149.69	1512.0	1.34444		
220	219.97	0.4690	156.82	1346.0			
230	230.02	0.5477	164.00	1205.0	1.43557		
240	240.02	0.6355	171.13	1084.0	1.47824		
250	250.05	0.7329	178.28	979.0	1.51917		
260	260.09	0.8405	185.45	887.8	1.55848		
270	270.11	0.9590	192.60	808.0	1.59634		
280	280.13	1.0889	199.75	738.0	1.63279		
285	285.14	1.1584	203.33	706.1	1.65055		
290	290.16	1.2311	206.91	676.1	1.66802		
295 298	295.17 298.18	1.3068	210.49 212.64	647.9 631.9	1.68515 1.69528		
300	300.19	1.3343	214.07	621.2	1.70203		
305	305.22	1.4686	217.67	596.0	1.71865		
310	310.24	1.5546	221.25	572.3	1.73498		
315	315.27	1.6442	224.85	549.8	1.75106		
320	320.29	1.7375	228.42	528.6	1.76690		
325	325.31	1.8345	232.02	508.4	1.78249		
330	330.34	1.9352	235.61	489.4	1.79783		
340	340.42	2.149	242.82	454.1	1.82790		
350	350.49	2.379	250.02	422.2	1.85708		
360	360.58	2.626	257.24	393.4	1.88543		
370	370.67	2.892	264.46	367.2			
380	380.77	3.176	271.69	343.4	1.94001		



## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### Department of Computer Science and Engineering (CSE)

MID SEMESTER EXAMINATION

WINTER SEMESTER, 2021-2022

**DURATION: 1 HOUR 30 MINUTES** 

**FULL MARKS: 75** 

#### **CSE 4373: Computer Programming and Applications**

Programmable calculators are not allowed. Do not write anything on the question paper.

Answer all 3 (three) questions. Marks of each question and corresponding CO and PO are written in the right margin with brackets.

1.	a)	What are the rules for naming identifiers? Distinguish between the following pair of data types (including their format specifiers for I/O) supported in C Programming Language:  i. float and double ii. short and long	3+4 (CO1) (PO1)
	b)	How can you compute the quotient and remainder between two integers in C? What is the purpose of unsigned type modifier? Write a C program to find the largest of three numbers without using any relational operators.	3+2+5 (CO2) (PO1)
	c)	What is the purpose of "const" keyword? Why should you use comment in a programming language? Distinguish between logical and relational operators in C.	2+3+3 (CO2) (PO1)
2.	a)	Distinguish between the nested if-else and if-else ladder in C. Write a 'C' program using simple if-else statements (without using any loop) that tries to guess a secret number in 3 attempts. In the first step the computer will set a random (secret) number from 0 to 9. Then a user (via input) will try to guess that secret number in 3 attempts; the user will win the game if any of the guesses is correct, and will lose otherwise.	3+10 (CO3) (PO2)
	b)	How does the switch statement work? What are the valid places where the programmer can apply Break and Continue control statement? Write a program in C that will sum all the numbers from 1 to 1000 while ignoring all numbers divisible by 3.	3+3+6 (CO3) (PO2)
3.	a)	What are the advantages of user-defined function? Explain the syntax of function prototype. Write a program in C to swap two numbers using a function.	3+2+4 (CO2) (PO2)
	b)	Explain the advantages and disadvantages of recursion. Write a program in C to Print Fibonacci Series using recursion.	4+6 (CO1) (PO1, PO2)
	c)	What is the output of the following program?	6
		void main()	(CO2) (PO2)
		int n=10;	(102)
		<pre>int f(int n);</pre>	
		printf("%d",f(n));	
		int f(int n)	
		{	
		if(n>0)	
		return (n+f (n-2));	

Figure 1: Code snippet for Question 3.(c)

Justify your answer with a flow chart.

#### Formulas: Hum 4721: All notations carry their usual meanings.

#### Time Value of money

$$i_{effective} = \left(1 + \frac{r}{m}\right)^m - 1 \quad i_{con/effective} = e^r - 1 \qquad i = \sqrt[n]{\frac{F}{P}} - 1$$
 
$$Estimated \quad n = \frac{72}{RoR\%} = \frac{72}{i}$$
 
$$F = P\left(1 + \frac{1}{k}\right)^{rkn} = P\left[\left(1 + \frac{1}{k}\right)^k\right]^{rn} \qquad F = Pe^{rn} = p(factor). \qquad r = ln(1+i)$$

Factor by which to multiply	Factor functional
the "Given"	symbol
$(1+i)^n$	(F/P, i%, n)
$(1+i)^{-n}$	(P/F, i%, n)
$[(1+i)^n-1]/i$	(F/A, i%, n)
$ \frac{[(1+i)^n - 1]/i}{[(1+i)^n - 1]} $	(P/A, i%, n)
$\frac{(1+i)^n - 1}{i(1+i)^n}$	(A/F, i%, n)
$\frac{1}{(1+i)^n-1}$	(A/P, i%, n)
$\frac{e^{rn}-1}{}$	$(F/\bar{A}, r\%, n)$
$\frac{e^{rn}-1}{re^{rn}}$	$(P/\bar{A},r\%,n)$
$\frac{r}{e^{rn}-1}$	$(\bar{A}/F, r\%, n)$
$\frac{re^{rn}}{e^{rn}-1}$	$(\bar{A}/P, r\%, n)$

$$F = \frac{G}{i} \left[ \frac{(1+i)^n - 1}{i} \right] - \frac{nG}{i} = \frac{G}{i} (F/G, i\%, n) - \frac{nG}{i}$$

$$A = \frac{G}{i} - \frac{nG}{i} \left[ \frac{i}{(1+i)^n - 1} \right] = G\left[ \frac{1}{i} - \frac{n}{(1+i)^n - 1} \right] = G(\frac{A}{G}, i\%, n)$$

$$P = A\left(\frac{P}{A}, i\%, n\right) = G\left[\frac{1}{i} - \frac{n}{(1+i)^n - 1}\right] \left[\frac{(1+i)^n - 1}{i(1+i)^n}\right]$$

$$= G\left\{\frac{1}{i}\left[\frac{(1+i)^{n-1}}{i(1+i)^n} - \frac{n}{(1+i)^n}\right]\right\} = G\frac{1}{i}\left(\frac{P}{G}, i\%, n\right)$$

$$= G\frac{1}{i}\left[\left(\frac{P}{A}, i\%, n\right) - n\left(\frac{P}{B}, i\%, n\right)\right]$$



TABLE D-15 10% compound interest factors

	Single Payment			Uniform Series			Uniform Gradient		
1	Compound amount factor F/P	Present worth factor P/F	Sinking fund factor A/F	Capital recovery factor A/P	Compound amount factor F/A	Present worth factor P/A	Gradient conversion factor A/G	Present worth factor P/G	n
1	1.1000	0.9091	1.000 00	1.100 00	1.000	0.909	0.000	0.000	
2	1.2100		0.476 19	0.576 19	2.100	1.736	0.476	0.826	
3	1.3310		0.302 11	0.402 11	3.310	2.487	0.937	2.329	
4	1.4641		0.215 47	0.315 47	4.641	3.170	1.381	4.378	
5	1.6105	0.6209	0.163 80	0.263 80	6.105	3.791	1.810	6.862	
6	1.7716	0.5645	0.129 61	0.229 61	7.716	4.355	2.224	9.684	
7	1.9487	0.5132	0.105 41	0.205 41	9.487	4.868	2.622	12.763	
8	2.1436	0.4665	0.087 44	0.187 44	11.436	5.335	3.004	16.029	
9	2.3579	0.4241	0.073 64	0.173 64	13.579	5.759	3.372	19.421	
10	2.5937	0.3855	0.062 75	0.162 75	15.937	6.144	3.725	22.891	
11	2.8531	0.3505	0.053 96	0.153 96	18.531	6.495	4.064	26.396	
12	3.1384		0.046 76	0.146 76	21.384	6.814	4.388	29.901	
13	3.4523	0.2897	0.040 78	0.140 78	24.523	7.103	4.699	33.377	
14	3.7975	0.2633	0.035 75	0.135 75	27.975	7.367	4.996	36.800	
15	4.1772	0.2394	0.031 47	0.131 47	31.772	7.606	5.279	40.152	
16	4.5950	0.2176	0.027 82	0.127 82	35.950	7.824	5.549	43.416	
17	5.0545	0.1978	0.024 66	0.124 66	40.545	8.022	5.807	46.582	
18	5.5599	0.1799	0.021 93	0.121 93	45.599	8.201	6.053	49.640	
19	6.1159	0.1635	0.019 55	0.119 55	51.159	8.365	6.286	52.583	
20	6.7275	0.1486	0.017 46	0.117 46	57.275	8.514	6.508	55.407	
21	7.4002	0.1351	0.015 62	0.115 62	64.002	8.649	6.719	58.110	
22	8.1403	0.1228	0.014 01	0.114 01	71.403	8.772	6.919	60.689	
23	8.9543	0.1117	0.012 57	0.112 57	79.543	8.883	7.108	63.146	
24	9.8497	0.1015	0.011 30	0.111 30	88.497	8.985	7.288	65.481 67.696	
25	10.8347	0.0923	0.010 17	0.110 17	98.347	9.077	7.458		
26		0.0839	0.009 16	0.109 16	109.182	9.161	7.619	69.794	
27		0.0763	0.008 26	0.108 26	121.100	9.237	7.770	71.777	
28		0.0693	0.007 45	0.107 45	134.210	9.307	7.914	73.650 75.415	
29		0.0630	0.006 73	0.106 73	148.631	9.370 9.427	8.049 8.176	77.077	
30		0.0573	0.006 08	0.106 08	164.494			78.640	
31		0.0521	0.005 50	0.105 50	181.943	9.479	8.296	80.108	
32		0.0474		0.104 97	201.138 222.252	9.526 9.569	8.409 8.515	81.486	
33		0.0431		0.104 50	245.477	9.609	8.615	82.777	
34		0.0391 0.0356		0.104 07 0.103 69	271.024	9.644	8.709	83.987	
35					442.593		9.096	88.953	
40		0.0221		0.102 26 0.101 39	718.905		9.374	92.454	
45		0.0137		0.101 39			9.570	94.889	
50		0.0053		0.100 53	1 880.591		9.708	96.562	
60		0.0033		0,100 33			9.802	97.701	
		0.0020		0.100 20			9.867	98.471	
65		0.0020					9.911	98.987	
70		0.0013					9.941	99.332	
80		0.0005					9.961	99.561	
8		0.0003					9.974	99.712	
90		0.0002					9.983	99.812	
9		0.0002					9.989	99.877	
10		0.0001					9.993	99.920	

B.Sc. Engg. IPE 3<sup>rd</sup> Semester

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### Department of Computer Science and Engineering (CSE)

MID SEMESTER EXAMINATION DURATION: 1 HOUR 30 MINUTES

WINTER SEMESTER, 2021-2022

**FULL MARKS: 75** 

#### **CSE 4373: Computer Programming and Applications**

Programmable calculators are not allowed. Do not write anything on the question paper.

Answer all <u>3 (three)</u> questions. Marks of each question and corresponding CO and PO are written in the right margin with brackets.

Evaluate the expression assigned to the variable 'ans' in Figure 1. Show the intermediate steps as 1. a) (CO4) well. (PO2) int a=1, b=2, c=3, d=5, ans; ans = a%5-a/b+c++\*++d;Figure 1: Code Snippet for 1(a) Write a program that will take three integers, n, m, and k as input. Then, it will take two regular 11 (CO2) matrices A and B of size  $(n \times m)$  Finally, it will evaluate the following expression. (PO2) C = A - k \* BOutline a step-by-step process describing how a computer reads, compiles, and executes a C (CO1) program. Use appropriate diagrams, if necessary. (PO2) Suppose for a game development project, you have to draw hollow triangular shapes of different 10 2. sizes. Write a program that takes a number n as input and print the patterns as shown in Figure 2. (CO3) (PO3)

Figure 2: Output form the program in Question 2(a) for n=2, n=3 and n=4

b) What would be the output of the code snippet in Figure 3?

int i;
for(i=1; i<100; i++)
{
 if(i%5==0 && i%3==0) continue;
 else if(i%3==0) printf("desh\n");
 else if(i%5==0) printf("bangla\n");
 if(i>21) break;
}

Figure 3: C program for snippet for Question 2(b)



c) Answer the following Questions:

i. What are the two major criteria to evaluate algorithms?

ii. What are the advantages of modular programming? Which features in C

Programming Language help to write modular programs?

3. a) Following is a buggy C program to convert Celsius into Fahrenheit. Briefly explain each bug in the program and debug it.

(CO1)

(PO1)

```
$include{stdio.h}
int main()
{
int celsius, fahrenheit, 1_f;
1_f = fahrenheit - 32
celcius = 1_f*9/5
    printf("%f", &celcius);
    return 0;
}
```

Figure 4: C program for Question 3(a)

b) Suppose you are developing a word processing software. As a part of that, you have to write a program that takes in a stream of characters as input and output the count of the numeric digits, upper-case letters, and lower-case letters as shown below. The program first takes an integer, **n** as input. Then, it takes a stream of **n** characters which are either digits upper-case or lower-case letters. The ASCII value of '0', 'A', 'a' is respectively 48, 65, and 97.

#### Input

15

sBc103Ghf456kJk

#### Output

Numeric Digits: 6

Upper-case Letters: 3

Lower-case Letters: 6

Write a program that approximates the sum of the first n terms of the first n terms of the following series. Here, n is an integer input by the user.  $1 + \frac{1}{1!} + \frac{1}{2!} + \frac{1}{3!} + \frac{1}{4!} + \dots$ (CO2)
(PO2)

(PO2)

(PO3)

(CO1) (PO1)

12.5

(CO2 (PO2

7.5 (CO1) (PO1)

B.Sc. Engg. (ME/IPE), 3<sup>rd</sup> Sem.

Date: September 30, 2022 (Morning)

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

# DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING

Mid-Semester Examination

Course No.: EEE 4381

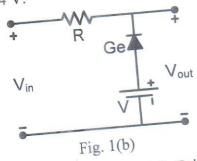
Course Title: Electronics and Digitization Techniques

Winter Semester, A. Y. 2021-2022 Time: 90 minutes

Full Marks: 75

There are 4 (four) questions. Question 1 is compulsory. Answer any 2 (two) questions from the other 03 (three). Marks in the margin indicate full marks. Do not write on this question paper.

- Define majority and minority carriers? Describe the differences between n-type and p-(CO1) (PO1) type semiconductor materials. 5 (CO2)
  - Sketch the input and output voltage wave shapes for the circuits in Fig. 1(b). Consider  $V_{in} = 10V_{peak}$ ,  $R = 1 \text{ k}\Omega$ , V = 4 V.



- Design a rectifier to convert 220 V AC to 10 V DC. Briefly explain each step of your 15 (CO3)design with necessary circuit diagram(s).
- Sketch the equivalent circuits and the forward characteristics for the equivalent models available for p-n junction diode. 2
  - Distinguish between a bipolar and unipolar device? Identify what kind of device a BJT is and justify your answer.
  - For the diode networks of Fig. 2(c), determine  $V_0$ ,  $I_1$ , and  $I_2$ .

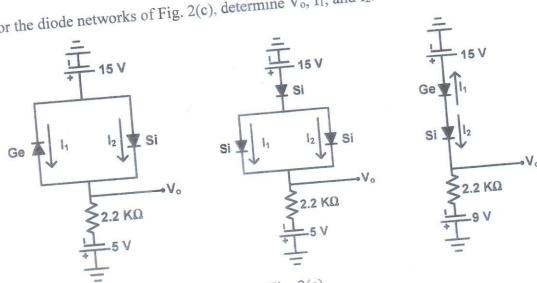
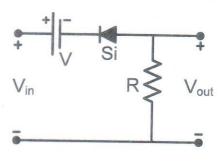


Fig. 2(c)

3. a) Sketch the input and output voltage wave shapes for the circuits in Fig. 3(a). Consider  $V_{in} = 20V_{peak}$ ,  $R = 1 \text{ k}\Omega$ , V = 7 V,  $C = 100 \text{ }\mu\text{F}$ .

12.5 (CO2)

(PO2)



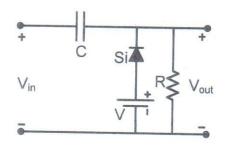


Fig: 3(a)

b) Sketch the common-emitter BJT configuration (for both npn and pnp) and indicate the polarity of the applied bias and resulting current directions. Also draw the collector characteristics and base characteristics.

12.5 (CO1)

(PO1)

4. a) Describe the transistor amplifying action with example.

5 (CO1)

b) Explain the significances of common base and common emitter amplification factors in

(PO1) 7.5

BJT amplifiers? Derive the relationship between them.

(CO1) (PO1)

c) Determine the levels of  $I_{CQ}$  and  $V_{CEQ}$  for the voltage-divider configuration of Fig. 4(c) using the exact and approximate techniques and compare solutions.

12.5 (CO2)

82 ΚΩ 5.6 ΚΩ

10 μF

V<sub>CEQ</sub>

22 ΚΩ 1.2 ΚΩ

Fig. 4(c)

PO2)

Program: B. Sc. in Industrial Production Engineering

Date: 29 September, 2022 Time: 10:30 a.m.- 12:00 p.m.

Semester: Winter

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

**Mid-Semester Examination** Course Number: ME 4503

Course Title: Mechanics of Machines

Winter Semester: 2021 - 2022

Full Marks:75

Time: 1.5 Hours

There are 3 (Three) questions. Answer all of them.

The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Assume reasonable value for missing data.

1. a. Figure 1 is showing the kinematic diagram of a front loader. Determine the mobility of the mechanism using kutzbach equation.

(8)(CO1)

(PO2)

(CO2)

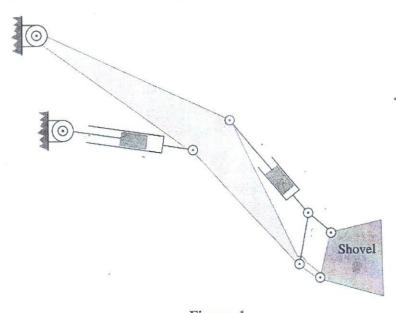


Figure. 1

b. A 4-tooth/in diametral pitch, 24-tooth pinion is to drive a 36-tooth gear. The (17) gears are cut on the 20° full-depth involute system. Find and tabulate the addendum, dedendum, clearance, circular pitch, base pitch, tooth thickness, pitch circle radii, base circle radii, lengths of paths of approach and recess, and contact ratio.

In Figure 2 axis y-y is fixed while axis x-x and z-z move with the arm. Gear 7 is fixed to the carrier. Gears 3 and 4, 5 and 6, and 8 and 9 are fixed together, (CO2) respectively. Gears 3 and 4 move with planetary motion. If the tooth numbers are  $N_2 = 16T$ ,  $N_3 = 20T$ ,  $N_4 = 22T$ ,  $N_5 = 14T$ ,  $N_6 = 15T$ ,  $N_7 = 36T$ ,  $N_8 = 20T$ ,  $N_9 = 41T$ , and  $N_{10} = 97T$ , determine the speed and direction of the output shaft.

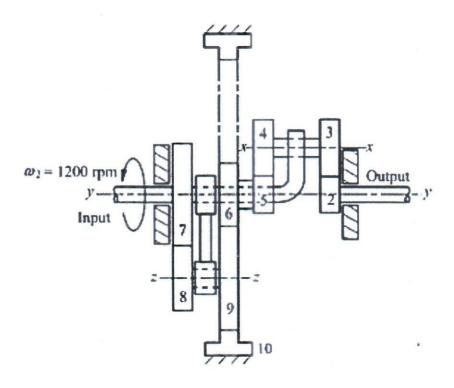


Figure. 2

3. Design a parabolic cam follower-displacement program to provide a dwell with (25) zero lift for the first 120° of the motion cycle, and a dwell at 0.8 in lift for cam (CO3) angles from 180° to 210°. Assume that the cam rotates with constant angular (PO3) velocity.

Program: B. Sc. in ME

B.Sc. in IPE

Semester: 5th

Date: 05 October, 2022

Time: 10:30 am - 12:00 pm

#### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)
DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination Course Number: Math 4511 Course Title: Numerical Analysis

Winter Semester: 2021 - 2022 Full Marks:75

Time: 1.5 HRS

There are **3** (**Three**) questions. Answer all questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Assume reasonable value for missing data

1. Figure 1 shows a uniform beam subject to a linearly increasing distributed (25) load. The equation for the resulting elastic curve is (see Figure 2) (CO1)

$$y = \frac{w_0}{120EL}(-x^5 + 2L^2x^3 - L^4x)$$
 (PO2)

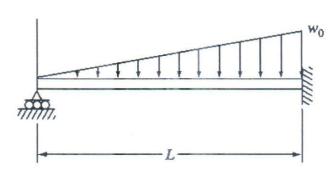
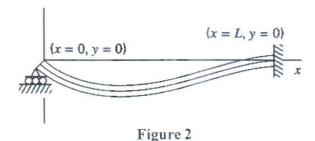


Figure 1



Page 1 of 2

(10)

Use *bisection* to determine the point of maximum deflection (that is, the value of x where dy/dx = 0). Then substitute this value into the above equation to determine the value of the maximum deflection. Use the following parameter values in your computation: L =600 cm, E =50,000 kN/cm<sup>2</sup>, I = 30,000 cm<sup>4</sup>, and  $w_0 = 2.5$  kN/cm

2. a) The power generated by a windmill varies with the wind speed. In an experiment, the following five measurements were obtained: (CO1) (PO2)

Wind speed(mph)	14	22	30	38	46
Electric Power (W)	320	490	540	500	480

Determine the *fourth-order* polynomial in the *Lagrange* form that passes through the points. Use the polynomial to calculate the power at a wind speed of 26 mph.

No need to expand the polynomial.

b) Use zero-through third-order Taylor series expansions to predict f(3) for

$$f(x) = 25x^3 - 6x^2 + 7x - 88$$
 (CO1)

using a base point at x = 1. Compute the true percent relative error for each approximation.

Use forward and backward difference approximations of O(h) and a centered difference approximation of  $O(h^2)$  to estimate the first derivative of the function. Evaluate the derivative at x = 2 using a step size of h = 0.2. Compare your results with the true value of the derivative

3. Solve the following system of four equations using the Gauss elimination (25) with partial pivoting (CO1) (PO2)

$$4x_1 - 2x_2 - 3x_3 + 6x_4 = 12$$

$$-6x_1 + 7x_2 + 6.5x_3 - 6x_4 = -6.5$$

$$x_1 + 7.5x_2 + 6.25x_3 + 5.5x_4 = 16$$

$$-12x_1 + 22x_2 + 15.5x_3 - x_4 = 17$$



Program: B. Sc. in Mechanical Engineering

Semester: 5th

Date: 03 October, 2022 Time: 10:30 am - 12:00 pm

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

#### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Semester Mid Examination Course Number: ME 4511 Course Title: Fluid Mechanics 2

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are **03** (three) questions. Answer all questions (choose option from question 1). The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Assume reasonable data for any missing values.

- 1. (a) Derive expression for force, torque and power of the Conical bearing. (10+15)
  - (b) "To achieve supersonic flow from a subsonic state in a duct, a converging-diverging area variation is necessary"- describe elaborately with all appropriate diagrams. (PO1)

    OR
  - (a) Derive an expression for force, torque and power of the collar bearing.
  - (b) "For supersonic flow through a duct, the area-velocity relationship is proportional"-describe the statement through mathematical proof and expression with appropriate diagrams.
- A shaft is supported by Journal, thrust and collar bearing as shown in Figure 1. The external and internal radii of a collar are 60 mm and 50 mm, respectively. An oil film of thickness 0.26 mm and viscosity of 0.1 N-s/m² is maintained for collar and thrust bearing. Journal bearing has film thickness half of the collar bearing with viscosity of 0.15 N-s/m². If the speed of the shaft is 700 rpm. Find the total force, total torque and total power absorbed in overcoming the viscous resistance.

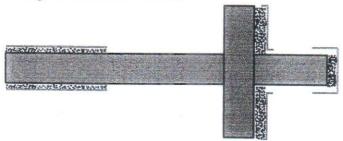


Figure 1

An open cylindrical tank having a diameter D is supported around its bottom circumference and is filled to a depth h with a liquid having a specific weight γ. The vertical deflection, d, of the center of the bottom is a function of D, h, t, γ, and E where t is the thickness of the bottom and E is the modulus of elasticity of the bottom material. Form the dimensionless groups describing this relationship.

[PO3]

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

MID Semester Examination

Course No.: ME 4513

Course Title: Principle of Heat and Mass Transfer

Winter Semester: A.Y. 2021-2022

Time: 1.0 Hour 30 Minutes

Full Marks: 75

There are **03** (**Three**) Questions. Answer all of them. Marks in the margin indicate full marks. Don't write on this question paper. Symbols carry their usual meanings. Assume reasonable values for any missing data. Programmable calculators are not allowed.

1.	(a)	<ul> <li>(i). Explain Thermal conductivity.</li> <li>(ii). Write five characteristics of thermal conductivity-its variation for different materials and under different conditions.</li> </ul>	[05] [CO2] [PO2]
	(b)	Heat is generated in a long wire of radius $r_0$ at a constant rate of $g_0$ per unit volume. The wire is covered with a plastic insulation layer. <i>Express</i> the heat flux boundary condition at the interface in terms of the heat generated.	[05] [CO2] [PO2]
	(c)	Consider steady 1D heat conduction in a plane wall with variable heat generation and constant thermal conductivity. The nodal network of the medium consists of nodes 0, 1, 2, 3, and 4 with a uniform nodal spacing of $\Delta x$ . Using the finite difference form of the first derivative, <i>state</i> the finite difference formulation of the boundary nodes for the case of uniform heat flux $q_0$ at the left boundary (node 0) and convection at the right boundary (node 4) with a convection coefficient of $h$ and an ambient temperature of $T_{\alpha}$ .	[05] [CO2] [PO2]
2.	(a)	Starting with an energy balance on a cylindrical shell volume element, $develop$ a correlation of the steady one-dimensional heat conduction equation for a long cylinder with constant thermal conductivity in which heat is generated at a rate of $g$ .	[10] [CO4] [PO4]
	(b)	Consider a sphere of radius $r_1$ whose surface temperature $T_1$ is maintained constant. The sphere is now insulated with a material whose thermal conductivity is k and outer radius is $r_2$ . Heat is lost from the sphere to the surrounding medium at temperature $T\alpha$ , with a convection heat transfer coefficient h. Verify that the critical radius of insulation for sphere is, $r_{cr}$ =2k/h.	[10] [CO4] [PO4]
	(c)	Design a temperature distribution profile and heat flow due to conduction in a circular conical rod with diameter as shown in Fig. 1 at any section given by D=cx where x is the distance measured from the apex of the cone and c is a certain numerical constant. Assume that lateral surface is well insulated, there is no internal heat generation and heat flow takes place under steady state conditions.	[10] [CO4] [PO4]
3.	(a)	A 150 mm steam pipe ( <b>Fig. 2</b> ) has inner diameter of 120 mm and outside diameter of 160 mm. It is insulated at the outside with asbestos. The steam temperature is 150°C and the air temperature is 20°C. h(steam side)=100 W/m $^2$ °C, h(air side)= 30 W/m $^2$ °C, k(asbestos)=0.8 W/m $^2$ °C and k(steel)= 42 W/m $^2$ °C. Calculate how thick the asbestos should be provided in order to limit the heat loses to 2.1 kW/m $^2$ .	[10] [CO3] [PO3]
	(b)	A long cylindrical bar (k=17.4 W/m°C, $\alpha$ =0.019 m²/h) of radius 80 mm comes out of oven at 830°C throughout and is cooled by quenching it in a large bath of 40°C coolant. The surface coefficient of heat transfer between the bar surface and the coolant is 180 W/m²°C. Determine: (i). The time taken by the shaft centre to reach 120°C. (ii). The surface temperature of the shaft when its centre temperature is 120°C. Also calculate the temperature gradient at the outside surface at the same instant of time.	[10] [CO3] [PO3]
	(c)	Consider a long concrete dam ( $k=0.6 \text{ W/m} \cdot \text{°C}$ , $\alpha=0.7 \text{ m}^2/\text{s}$ ) of triangular cross section (Fig. 3) whose exposed surface is subjected to solar heat flux of $q_s=800 \text{ W/m}^2$ and to convection and radiation to the environment at $2.5^{\circ}\text{C}$ with a combined heat transfer coefficient of 30 W/m <sup>2</sup> ·°C. The 2-m-high vertical section of the dam is	[10] [CO3]

25°C with a combined heat transfer coefficient of 30 W/m<sup>2</sup>.°C. The 2-m-high vertical section of the dam is

subjected to convection by water at 15°C with a heat transfer coefficient of 150 W/m<sup>2</sup>.°C, and heat transfer through the 2-m-long base is considered to be negligible. Using the finite difference method with a mesh size of  $\Delta x = \Delta y = 1$  m and assuming steady two-dimensional heat transfer, determine the temperature of the top,

middle, and bottom of the exposed surface of the dam.



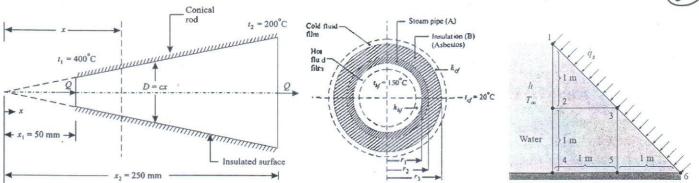
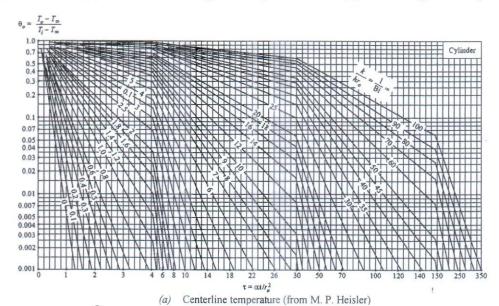
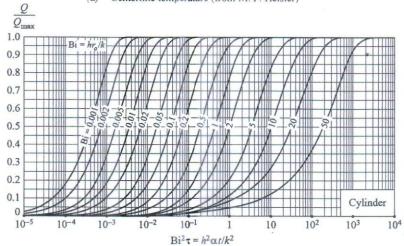


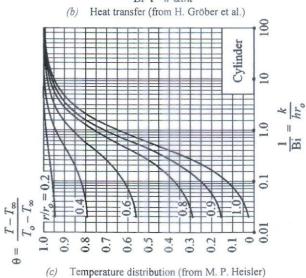
Fig: 1-For Question No 2(c)

Fig: 2-For Question No 3(a)

Fig: 3-For Question No 3(c)









Program: B. Sc. in Mechanical Engineering/

B. Sc. in Technical Education

Semester: 5th

Date: 30th September, 2022 (Friday)

Time: 10:30 am - 12:00 pm (Morning)

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid-Semester Examination Course Number: IPE 4521 Course Title: Manufacturing Process Winter Semester: 2021 - 2022 Full Marks: 75

Time: 1 hour 30 Minutes

There are **4 (four)** questions. Question no. **1** is alternative to question no. **2**. Answer **3 (three)** questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets.

1.	a)	Define pattern. Write brief note on the pattern allowances that can be quantitatively specified.	(10) (CO1) (PO1)
	b)	Explain some of the moulding material and gas defects of a sand casting with their causes and defects.	(10) (CO1) (PO1)
	c)	Mention some advantages and disadvantages of permanent mould casting.	(05) (CO1) (PO1)
		OR	
2.	a)	Briefly discuss about die casting process with its advantages and disadvantages.	(10) (CO1) (PO1)
	b)	Mention the factors responsible for different types of chip formation.	(08) (CO1) (PO1)
	c)	What is simple indexing and compound indexing? Explain with examples.	(07) (CO1) (PO1)

3.	a)	A sand specimen with a permeability number of 140 takes 45 seconds to pass 2000 cm <sup>3</sup> of air at a pressure of 5g/cm <sup>2</sup> . Calculate the height of the sand specimen.	(05) (CO2) (PO2)
	b)	Shear angle can be measured by measuring chip thickness, depth of cut and rake angle of tool. Prove this statement.	(10) (CO2) (PO2)
	c)	Is it possible to obtain a casting of a solid bar by centrifugal casting? Give reasons in support of your answer.	(05) (CO2) (PO2)
	d)	At what r.p.m. should a lathe be run to give a cutting speed of 60 m/min, when turning a rod of diameter of 42 mm and length 500 mm. Hence, find out machining time for feed of 0.8 mm/min.	(05) (CO2) (PO2)
4.	a)	Explain the quick return mechanism of a shaper machine with necessary diagram.	(10) (CO1) (PO1)
	b)	Describe with necessary diagram the working principle of a lathe apron. Write a short note on Taper Turning.	(10) (CO1) (PO1)
	c)	Explain different types of operations that can be performed on a drilling machine.	(05) (CO1) (PO1)

Program: BSc. Eng. (ME/IPE) Semester: 5th Semester

Date: 4 October 2022 Time: 10:30 am - 12:00 pm

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid-Semester Examination

Winter Semester, A.Y. 2021-2022 : 75

Full Marks

Course Number: IPE 4531 Course Title: Probability and Statistics

Time

: 11/2 Hours

There are 3 (Three) questions. Answer all of them. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the right column.

Assume reasonable values if required. Selected formulas and charts are provided at the end of the question.

1 Suppose you were working in the quality department of a lubricant company. 25 Which sampling method would you use for quality control? Explain with reasons. CO1 Raw data on the weight in gram of a lubricant product collected from that factory PO1, is tabled below: PO<sub>2</sub>

198	147	286
155	236	267
213	224	191
257	193	208
170	181	226

- Make the data into appropriate classes and then prepare a frequency table. i.
- Determine the Range, Mean, Median, Mode and Standard Deviation from ii. grouped data.
- iii. Draw a stem and leaf diagram using the above data set.
- According to Journal of Engineering Progress, approximately 30% of all pipework failures in chemical plants are caused by operator error. CO<sub>2</sub> (i) Determine the probability that out of the next 10 pipework failures at least 5 PO<sub>3</sub> are due to operator error.
  - (ii) Calculate the probability that no more than 4 out of 20 such failures are due to operator error.
  - Potholes on a highway can be a serious problem, and are in constant need of repair. 6 With a particular type of terrain and make of concrete, past experience CO2 suggests that there are, on the average 2 potholes per mile after a certain amount PO3 of usage.
    - Determine the probability that no pothole will appear in a section of 1 i.
    - ii. Calculate the probability that no more than one potholes will occur in a given section of 5 miles.
    - Mention main reason for using a specific probability distribution for iii. solving this problem.

- c) Lately five women and eight men applied for a job to a manufacturing company. 7
  The personnel manager claimed that the applicants were so equally qualified that CO2
  he made the selection of the three people hired totally by random process. The PO3
  selection resulted in three men and no women being selected. The women have
  filed discrimination charges against the company. Based on probability, what
  would you conclude about the suit? Discuss.
- d) MPE dept has 120 students at 3rd year. Among them, 30 students took Solar energy and 40 students took Material Handling. There are 10 students who took both Solar energy and Material handling. If a 3rd year MPE student is chosen at random, what is the probability that the student has taken Solar energy? What is the probability that the student has taken solar energy given that Materials handling also taken prior to that.
- Banks affiliated with IUT would like to find out the best estimate of the percentage of IUT students using internet banking. Banks want the estimate to be within .10 CO2 of the population proportion, the desired level of confidence is 95 percent, and no estimate is available for the population proportion. Using this information, determine the required sample size. Then using this sample size, how would you find out the best estimate of the percentage of IUT students using internet banking and confidence interval? Explain.
  - b) Gauges are used to reject all components for which a certain dimension is not 7 within the specification  $1.50 \pm d$ . It is known that this measurement is normally CO2 distributed with mean 1.50 and standard deviation 0.2. Determine the value of d PO3 such that the specifications "cover" 95% of the measurements
  - c) The average life of a certain type of small motor is 10 years with a standard 6 deviation of 2 years. The Manufacturer replaces free all motors that fail while CO2 under guarantee. If she is willing to replace only 3% of The motors that fail, how long a guarantee should be offered? Assume that the life time of a motor follows a normal distribution
  - d) The average grade for an exam is 74, and the standard deviation is 7. If 15% of The class is given As, and the grades are curved to follow a normal distribution, What is the cutoff mark to get A grade, i.e. you will get A grade when your earned mark is equal or larger than this cutoff mark?

Formulas:::  $n = p(1 - p) \left(\frac{z}{E}\right)^2$ 

Median:

$$s = \sqrt{\frac{n\sum_{i}^{n} (f_{i}X_{i}^{2}) - (\sum_{i}^{n} f_{i}X_{i})^{2}}{n-1}} \qquad M_{d} = L + \left(\frac{N_{2} - n_{b}}{n_{w}}\right) i \qquad = R / (1 + 3.322 \text{ logn})$$

$$b(x; n, P) = {}^{n}C_{x} * P^{x} * (1 - P)^{n-x}$$

$$P(x; \mu) = (e^{-\mu})*(\mu^{x}) / x!$$

$$h(x; N, n, k) = {\binom{k}{C_x}}^* {\binom{N-k}{C_{n-x}}} / {\binom{N}{C_n}}$$



Table A.3 Areas under the Normal Cur	Table	A.3 Areas	under the	Normal	Curve
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ie A.5 Al	reas under	the Norn	nai Curve				0 2		
.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0003	0.0002
0.0005	0.0005	0.0005	0.0004	0.0004	0.0004	0.0004	0.0004	0.0004	0.0003
			0.0006	0.0006	0.0006	0.0006	0.0005	0.0005	0.0005
			0.0009	0.0008	0.0008	0.0008	0.0008	0.0007	0.0007
0.0013	0.0013	0.0013	0.0012	0.0012	0.0011	0.0011	0.0011	0.0010	0.0010
0.0019	0.0018	0.0018	0.0017	0.0016	0.0016	0.0015	0.0015	0.0014	0.0014
0.0026	0.0025	0.0024	0.0023	0.0023	0.0022	0.0021	0.0021	0.0020	0.0019
0.0035	0.0034	0.0033	0.0032	0.0031	0.0030	0.0029	0.0028	0.0027	0.0026
			0.0043	0.0041	0.0040	0.0039	0.0038	0.0037	0.0036
0.0062	0.0060	0.0059	0.0057	0.0055	0.0054	0.0052	0.0051	0.0049	0.0048
0.0082	0.0080	0.0078	0.0075	0.0073	0.0071	0.0069	0.0068	0.0066	0.0064
0.0107	0.0104	0.0102	0.0099	0.0096	0.0094	0.0091	0.0089	0.0087	0.0084
				0.0125	0.0122	0.0119	0.0116	0.0113	0.0110
									0.0143
0.0228		0.0217	0.0212	0.0207	0.0202	0.0197	0.0192	0.0188	0.0183
0.0287		0.0274	0.0268	0.0262	0.0256	0.0250	0.0244	0.0239	0.0233
		0.0344	0.0336	0.0329	0.0322	0.0314	0.0307	0.0301	0.0294
									0.0367
									0.0455
				0.0618	0.0606	0.0594	0.0582	0.0571	0.0559
				0.0749	0.0735	0.0721	0.0708	0.0694	0.0681
									0.0823
									0.0985
									0.1170
									0.1379
									0.1611
									0.1867
									0.2148
									0.2451
									0.2776
									0.3121
									0.3483
									0.3859
									0.4247
0.5000	0.4960	0.4920	0.4880	(0.4840)	0.4801	0.4761	0.4721	0.4681	0.4641
	.00 0.0003 0.0005 0.0007 0.0010 0.0013 0.0019 0.0026 0.0035 0.0047 0.0062 0.0082 0.0107 0.0139 0.0179 0.0228	.00         .01           0.0003         0.0003           0.0005         0.0005           0.0007         0.0007           0.0010         0.0009           0.0013         0.0013           0.0026         0.0025           0.0035         0.0034           0.0047         0.0045           0.0062         0.0060           0.0082         0.0080           0.0107         0.0104           0.0139         0.0136           0.0179         0.0174           0.0228         0.0222           0.0287         0.0281           0.0359         0.0351           0.0446         0.0436           0.0548         0.0537           0.0668         0.0655           0.0808         0.0793           0.0968         0.0951           0.1151         0.1131           0.1587         0.1562           0.1841         0.1814           0.2119         0.2090           0.2420         0.2389           0.2743         0.2709           0.3821         0.3783           0.4207         0.4168           0.4562 <td>.00         .01         .02           0.0003         0.0003         0.0003           0.0005         0.0005         0.0005           0.0007         0.0006         0.0009           0.0010         0.0009         0.0009           0.0013         0.0013         0.0018           0.0026         0.0025         0.0024           0.0035         0.0034         0.0033           0.0047         0.0045         0.0044           0.0062         0.0060         0.0059           0.0082         0.0080         0.0078           0.0107         0.0104         0.0102           0.0139         0.0136         0.0132           0.0179         0.0174         0.0170           0.0228         0.0222         0.0217           0.0287         0.0281         0.0274           0.0359         0.0351         0.0344           0.0466         0.0436         0.0427           0.0548         0.0537         0.0526           0.0668         0.0655         0.0643           0.0808         0.0793         0.0778           0.0968         0.0951         0.0934           0.1151         0.1131</td> <td>.00         .01         .02         .03           0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0006         0.0006           0.0010         0.0009         0.0009         0.0009           0.0013         0.0013         0.0013         0.0012           0.0019         0.0018         0.0018         0.0017           0.0026         0.0025         0.0024         0.0023           0.0035         0.0034         0.0033         0.0032           0.0047         0.0045         0.0044         0.0043           0.0062         0.0060         0.0059         0.0057           0.0082         0.0080         0.0078         0.0075           0.0107         0.0104         0.0102         0.0099           0.0139         0.0136         0.0132         0.0129           0.0179         0.0174         0.0170         0.0166           0.0228         0.0222         0.0217         0.0212           0.0287         0.0281         0.0274         0.0268           0.0359         0.0351         0.0344         0.0336           0.0446         0.0436         0.0427         0.0418<!--</td--><td>0.0003         0.0003         0.0003         0.0003         0.0004           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0009         0.0008           0.0013         0.0013         0.0013         0.0017         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023           0.0035         0.0034         0.0033         0.0032         0.0031           0.0047         0.0045         0.0044         0.0043         0.0041           0.0062         0.0060         0.0059         0.0057         0.0055           0.0082         0.0080         0.0078         0.0075         0.0073           0.0107         0.0104         0.0102         0.0099         0.0096           0.0139         0.0136         0.0132         0.0129         0.0125           0.0179         0.0174         0.0170         0.0166         0.0162           0.0228         0.0222         0.0217         0.0212         0.0207           0.0287         0.0281         0.0274         0.026</td><td>.00         .01         .02         .03         .04         .05           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008           0.0013         0.0013         0.0013         0.0012         0.0012         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071           0.0107         0.0104         0.0102         0.0099         0.0066         0.0094</td><td>.00         .01         .02         .03         .04         .05         .06           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008         0.0008           0.0013         0.0013         0.0012         0.0012         0.0011         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016         0.0015           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022         0.0021           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030         0.0029           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040         0.0039           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054         0.0052           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071         0.0069           0.0179         0.0136</td><td>.00         .01         .02         .03         .04         .05         .06         .07           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0004         0.0004         0.0004         0.0004         0.0006         0.0008         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011</td><td>.00         .01         .02         .03         .04         .05         .06         .07         .08           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0005         0.0005         0.0003         0.0006         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0021         0.0021         0.0021         0.0021         0.0021         0.0022         0.0022         0.0022         0.0022</td></td>	.00         .01         .02           0.0003         0.0003         0.0003           0.0005         0.0005         0.0005           0.0007         0.0006         0.0009           0.0010         0.0009         0.0009           0.0013         0.0013         0.0018           0.0026         0.0025         0.0024           0.0035         0.0034         0.0033           0.0047         0.0045         0.0044           0.0062         0.0060         0.0059           0.0082         0.0080         0.0078           0.0107         0.0104         0.0102           0.0139         0.0136         0.0132           0.0179         0.0174         0.0170           0.0228         0.0222         0.0217           0.0287         0.0281         0.0274           0.0359         0.0351         0.0344           0.0466         0.0436         0.0427           0.0548         0.0537         0.0526           0.0668         0.0655         0.0643           0.0808         0.0793         0.0778           0.0968         0.0951         0.0934           0.1151         0.1131	.00         .01         .02         .03           0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0006         0.0006           0.0010         0.0009         0.0009         0.0009           0.0013         0.0013         0.0013         0.0012           0.0019         0.0018         0.0018         0.0017           0.0026         0.0025         0.0024         0.0023           0.0035         0.0034         0.0033         0.0032           0.0047         0.0045         0.0044         0.0043           0.0062         0.0060         0.0059         0.0057           0.0082         0.0080         0.0078         0.0075           0.0107         0.0104         0.0102         0.0099           0.0139         0.0136         0.0132         0.0129           0.0179         0.0174         0.0170         0.0166           0.0228         0.0222         0.0217         0.0212           0.0287         0.0281         0.0274         0.0268           0.0359         0.0351         0.0344         0.0336           0.0446         0.0436         0.0427         0.0418 </td <td>0.0003         0.0003         0.0003         0.0003         0.0004           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0009         0.0008           0.0013         0.0013         0.0013         0.0017         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023           0.0035         0.0034         0.0033         0.0032         0.0031           0.0047         0.0045         0.0044         0.0043         0.0041           0.0062         0.0060         0.0059         0.0057         0.0055           0.0082         0.0080         0.0078         0.0075         0.0073           0.0107         0.0104         0.0102         0.0099         0.0096           0.0139         0.0136         0.0132         0.0129         0.0125           0.0179         0.0174         0.0170         0.0166         0.0162           0.0228         0.0222         0.0217         0.0212         0.0207           0.0287         0.0281         0.0274         0.026</td> <td>.00         .01         .02         .03         .04         .05           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008           0.0013         0.0013         0.0013         0.0012         0.0012         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071           0.0107         0.0104         0.0102         0.0099         0.0066         0.0094</td> <td>.00         .01         .02         .03         .04         .05         .06           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008         0.0008           0.0013         0.0013         0.0012         0.0012         0.0011         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016         0.0015           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022         0.0021           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030         0.0029           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040         0.0039           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054         0.0052           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071         0.0069           0.0179         0.0136</td> <td>.00         .01         .02         .03         .04         .05         .06         .07           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0004         0.0004         0.0004         0.0004         0.0006         0.0008         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011</td> <td>.00         .01         .02         .03         .04         .05         .06         .07         .08           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0005         0.0005         0.0003         0.0006         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0021         0.0021         0.0021         0.0021         0.0021         0.0022         0.0022         0.0022         0.0022</td>	0.0003         0.0003         0.0003         0.0003         0.0004           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0009         0.0008           0.0013         0.0013         0.0013         0.0017         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023           0.0035         0.0034         0.0033         0.0032         0.0031           0.0047         0.0045         0.0044         0.0043         0.0041           0.0062         0.0060         0.0059         0.0057         0.0055           0.0082         0.0080         0.0078         0.0075         0.0073           0.0107         0.0104         0.0102         0.0099         0.0096           0.0139         0.0136         0.0132         0.0129         0.0125           0.0179         0.0174         0.0170         0.0166         0.0162           0.0228         0.0222         0.0217         0.0212         0.0207           0.0287         0.0281         0.0274         0.026	.00         .01         .02         .03         .04         .05           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0004           0.0007         0.0007         0.0006         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008           0.0013         0.0013         0.0013         0.0012         0.0012         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071           0.0107         0.0104         0.0102         0.0099         0.0066         0.0094	.00         .01         .02         .03         .04         .05         .06           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003           0.0005         0.0005         0.0004         0.0004         0.0006         0.0006         0.0006           0.0010         0.0009         0.0009         0.0008         0.0008         0.0008           0.0013         0.0013         0.0012         0.0012         0.0011         0.0011           0.0019         0.0018         0.0018         0.0017         0.0016         0.0016         0.0015           0.0026         0.0025         0.0024         0.0023         0.0023         0.0022         0.0021           0.0035         0.0034         0.0033         0.0032         0.0031         0.0030         0.0029           0.0047         0.0045         0.0044         0.0043         0.0041         0.0040         0.0039           0.0062         0.0060         0.0059         0.0057         0.0055         0.0054         0.0052           0.0082         0.0080         0.0078         0.0075         0.0073         0.0071         0.0069           0.0179         0.0136	.00         .01         .02         .03         .04         .05         .06         .07           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0004         0.0004         0.0004         0.0004         0.0006         0.0008         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011	.00         .01         .02         .03         .04         .05         .06         .07         .08           0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0003         0.0004         0.0005         0.0005         0.0003         0.0006         0.0008         0.0008         0.0008         0.0008         0.0001         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0011         0.0021         0.0021         0.0021         0.0021         0.0021         0.0022         0.0022         0.0022         0.0022



Table A.3 (continued) Areas under the Normal Curve

Tat	ne A.3 (	continued)	Aleas III	idel the r	iormai Ct	live				
z	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
0.0	0.5000	0.5040	0.5080	0.5120	0.5160	0.5199	0.5239	0.5279	0.5319	0.5359
0.1	0.5398	0.5438	0.5478	0.5517	0.5557	0.5596	0.5636	0.5675	0.5714	0.5753
0.2	0.5793	0.5832	0.5871	0.5910	0.5948	0.5987	0.6026	0.6064	0.6103	0.6141
0.3	0.6179	0.6217	0.6255	0.6293	0.6331	0.6368	0.6406	0.6443	0.6480	0.6517
0.4	0.6554	0.6591	0.6628	0.6664	0.6700	0.6736	0.6772	0.6808	0.6844	0.6879
0.5	0.6915	0.6950	0.6985	0.7019	0.7054	0.7088	0.7123	0.7157	0.7190	0.7224
0.6	0.7257	0.7291	0.7324	0.7357	0.7389	0.7422	0.7454	0.7486	0.7517	0.7549
0.7	0.7580	0.7611	0.7642	0.7673	0.7704	0.7734	0.7764	0.7794	0.7823	0.7852
0.8	0.7881	0.7910	0.7939	0.7967	0.7995	0.8023	0.8051	0.8078	0.8106	0.8133
0.9	0.8159	0.8186	0.8212	0.8238	0.8264	0.8289	0.8315	0.8340	0.8365	0.8389
1.0	0.8413	0.8438	0.8461	0.8485	0.8508	0.8531	0.8554	0.8577	0.8599	0.8621
1.1	0.8643	0.8665	0.8686	0.8708	0.8729	0.8749	0.8770	0.8790	0.8810	0.8830
1.2	0.8849	0.8869	0.8888	0.8907	0.8925	0.8944	0.8962	0.8980	0.8997	0.9015
1.3	0.9032	0.9049	0.9066	0.9082	0.9099	0.9115	0.9131	0.9147	0.9162	0.9177
1.4	0.9192	0.9207	0.9222	0.9236	0.9251	0.9265	0.9279	0.9292	0.9306	0.9319
1.5	0.9332	0.9345	0.9357	0.9370	0.9382	0.9394	0.9406	0.9418	0.9429	0.9441
1.6	0.9452	0.9463	0.9474	0.9484	0.9495	0.9505	0.9515	0.9525	0.9535	0.9545
1.7	0.9554	0.9564	0.9573	0.9582	0.9591	0.9599	0.9608	0.9616	0.9625	0.9633
1.8	0.9641	0.9649	0.9656	0.9664	0.9671	0.9678	0.9686	0.9693	0.9699	0.9706
1.9	0.9713	0.9719	0.9726	0.9732	0.9738	0.9744	0.9750	0.9756	0.9761	0.9767
2.0	0.9772	0.9778	0.9783	0.9788	0.9793	0.9798	0.9803	0.9808	0.9812	0.9817
2.1	0.9821	0.9826	0.9830	0.9834	0.9838	0.9842	0.9846	0.9850	0.9854	0.9857
2.2	0.9861	0.9864	0.9868	0.9871	0.9875	0.9878	0.9881	0.9884	0.9887	0.9890
2.3	0.9893	0.9896	0.9898	0.9901	0.9904	0.9906	0.9909	0.9911	0.9913	0.9916
2.4	0.9918	0.9920	0.9922	0.9925	0.9927	0.9929	0.9931	0.9932	0.9934	0.9936
2.5	0.9938	0.9940	0.9941	0.9943	0.9945	0.9946	0.9948	0.9949	0.9951	0.9952
2.6	0.9953	0.9955	0.9956	0.9957	0.9959	0.9960	0.9961	0.9962	0.9963	0.9964
2.7	0.9965	0.9966	0.9967	0.9968	0.9969	0.9970	0.9971	0.9972	0.9973	0.9974
2.8	0.9974	0.9975	0.9976	0.9977	0.9977	0.9978	0.9979	0.9979	0.9980	0.9981
2.9	0.9981	0.9982	0.9982	0.9983	0.9984	0.9984	0.9985	0.9985	0.9986	0.9986
3.0	0.9987	0.9987	0.9987	0.9988	0.9988	0.9989	0.9989	0.9989	0.9990	0.9990
3.1	0.9990	().9991	0.9991	0.9991	0.9992	0.9992	0.9992	0.9992	0.9993	0.9993
3.2	0.9993	0.9993	0.9994	0.9994	0.9994	0.9994	0.9994	0.9995	0.9995	0.9995
3.3	0.9995	0.9995	0.9995	0.9996	0.9996	0.9996	0.9996	0.9996	0.9996	0.9997
3.4	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9997	0.9998
-										



Program: B. Sc. in Industrial and Production

Engineering

Semester: Winter

Date: 30 September, 2022

Time: 10:30 am - 12:00pm

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

·· ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Semester Mid Examination

Course Number: IPE 4539

Course Title: Engineering Economy and Finance

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are 3 (THREE) questions. Answer 3 (THREE) questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Formula sheet and relevant tables are provided.

1. Discuss the benefits of Engineering Economy to engineers.

(10 Marks)

b. Elaborate on the engineering economy analysis procedures.

(15 Marks)

(CO1)

(PO 1)

Ahmed borrows USD 75,000 from a bank for 1 year at 8% interest for 2.

(CO1)

a new industrial machine.

(PO 1)

Solve the:

i. Interest rate

(3 Marks)

ii. Amount due after1 year

(4 Marks)

b. A company manger purchases a machine for USD 50,000. The annual (10 Marks) operating cost is USD 3,500 including the cost of maintenance.

However, the machine needs to be calibrated in year 3 for a cost of USD

5,000 and later be sold at year 10 for an amount of USD 10,000.

Construct the cash flow diagram.



- c. i. USD 200,000 lent for 4 years at simple i = 5% per year. (3 Marks)

  Calculate the simple interest after 3 years.
  - ii. USD 200,000 lent for 4 years at i = 5% per year compounded. (5 Marks) Calculate the compound interest rate after 3 years.
- a. A start-up company made an investment of USD 100 million that is (CO 2) expected to generate USD 50 million per year in revenue for the (PO 2) duration of 6 years. A 10% per year time value of money is applied here.
  - i. Solve for the equivalent future worth of the estimated revenues after (5 Marks)6 years at 10% per year.
  - ii. As result of economic downturn, the company predicted that the (10 Marks) earning will drop to 5.5% per year on its money from the previously anticipated 10% per year.
    Calculate the revenue per year based on the revised rate of 5.5%.
  - b. A Petro-chemical plant has upgraded its gas emission control panel with (CO 2) a cost of USD10,000 and is expected to last for 10 years having a (PO 2) salvage value of USD 500. The cost of maintenance is expected to be at USD 1,500 during the first year and increasing by 9% per year thereafter. (10 Marks)
    Calculate by hand the equivalent present worth of the modification and maintenance cost at a rate of 6% per year.



	Single Pay	ments		Uniform Seri	es Payments		Arithmetic	Gradients
n	Compound Amount F/P	Present Worth P/F	Sinking Fund A/F	Compound Amount F/A	Capital Recovery A/P	Present Worth P/A	Gradient Present Worth P/G	Gradient Uniform Series A/G
1	1.0500	0.9524	1.00000	1.0000	1.05000	0.9524		
2	1.1025	0.9070	0.48780	2.0500	0.53780	1.8594	0.9070	0.4378
3	1.1576	0.8638	0.31721	3.1525	0.36721	2.7232	2.6347	0.9675
4	1.2155	0.8227	0.23201	4.3101	0.28201	3.5460	5.1028	1,4391
5	1.2763	0.7835	0.18097	5.5256	0.23097	4.3295	8.2369	1.9025
6	1.3401	0.7462	0.14702	6,8019	0.19702	5.0757	11.9680	2.3579
7	1.4071	0.7107	0.12282	8.1420	0.17282	5.7864	16.2321	2.8052
8	1.4775	0.6768	0.10472	9,5491	0.15472	6.4632	20.9700	3.2445
9	1.5513	0.6446	0.09069	11.0266	0.14069	7.1078	26.1268	3,6758
10	1.6289	0.6139	0.07950	12.5779	0.12950	7.7217	31.6520	4.0991
11	1.7103	0.5847	0.07039	14.2068	0.12039	8.3064	37.4988	4.5144
12	1.7959	0.5568	0.06283	15.9171	0.11283	8.8633	13.6241	4.9219

	Single Pay	ments	100	Uniform Seri	es Payments		Arithmetic	Gradients
n	Compound Amount F/P	Present Worth P/F	Sinking Fund A/F	Compound Amount F/A	Capital Recovery A/P	Present Worth P/A	Gradient Present Worth P/G	Gradient Uniform Series A/G
1	1.0600	0.9434	1.00000	1 0000	1.06000	0.9434		
2	1.1236	0.8900	0.48544	2.0600	0.54544	1.8334	0.8900	0.4854
3	1.1910	0.8396	0.31411	3.1836	0.37411	2.6730	2.5692	0.9612
4	1.2625	0.7921	0.22859	4.3746	0.28859	3.4651	4.9455	1.4272
5	1.3382	0.7473	0.17740	5.6371	0.23740	4.2124	7.9345•	1.8836
6	1.4185	0.7050	0.14336	6.9753	0.20336	4.9173	11.4594	2.3304
7	1.5036	0.6651	0.11914	8.3938	0.17914	5.5824	15.4497	2.7676
8	1.5938	0.6274	0.10104	9.8975	0 16104	6.2098	19.8416	3.1952
9	1.6895	0.5919	0.08702	11.4913	0.14702	6.8017	24.5768	3.6133
10	1.7908	0.5584	0.07587	13.1808	0.13587	7.3601	29.6023	4.0220
11	1.8983	0.5268	0.06679	14.9716	0.12679	7.8869	34.8702	4.4213
12	2.0122	0.4970	0.05928	16.8699	0.11928	8.3838	40.3369	4.8113

	Single Pay	ments		Uniform Seri	es Payments		Arithmetic	Gradients
n	Compound Amount F/P	Present Worth P/F	Sinking Fund A/F	Compound Amount F/A	Capital Recovery A/P	Present Worth P/A	Gradient Present Worth P/G	Gradient Uniform Series A/G
1	1.1000	0.9091	1.00000	1.0000	1.10000	0.9091		
2	1.2100	0.8264	0.47619	2.1000	0.57619	1.7355	0.8264	0.4762
3	1.3310	0.7513	0.30211	3.3100	0.40211	2.4869	2.3291	0.9366
4	1.4641	0.6830	0.21547	4.6410	0.31547	3.1699	4.3781	1.3812
5	1.6105	0.6209	0.16380	6.1051	0.26380	3.7908	6.8618	1.8101
6	1.7716	0.5645	0.12961	7.7156	0.22961	4.3553	9.6842	2.2236
7	1.9487	0.5132	0.10541	9.4872	0.20541	4.8684	12.7631	2.6216
8	2.1436	0.4665	0.08744	11.4359	0.18744	5.3349	16.0287	3.0045
9	2.3579	0.4241	0.07364	13.5795	0.17364	5.7590	19.4215	3.3724
10	2.5937	0.3855	0.06275	15.9374	0.16275	6.1416	22.8913	3.7255
11	2.8531	0.3505	0.05396	18.5312	0.15396	6.4951	26,3963	4.0641
12	3.1384	0.3186	0.04676	21.3843	0.14676	6.8137	29.9012	4.3884

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### FORMULA SHEET

$$F=P(1+i)^n$$

$$P = F(1 + i)^{-n}$$

$$P = A \frac{(1+i)^n - 1}{i(1+i)^n}$$

$$A = P \frac{i(1+i)^n}{(1+i)^n - 1}$$

$$F = A \frac{(1+i)^n - 1}{i}$$

$$A = F \frac{i}{(1+i)^n - 1}$$

$$f = f_1 + \frac{(x - x_1)}{(x_2 - x_1)} (f_2 - f_1)$$

$$P_G = (P/G, i, n) = \frac{(1 + i)^n - in - 1}{i^2(1 + i)^n}$$

$$F_G = G\left[\left(\frac{1}{i}\right)\left(\frac{(1+i)^n-1}{i}\right)-n\right]$$

$$A_G = G \ \left[ \frac{1}{i} - \frac{n}{(1+i)^n - 1} \right]$$

# ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC) DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

MID Semester Examination

Course No.: ME 4555

Course Title: Fluid Mechanics and Machinery

Winter Semester: A.Y. 2021-2022

Time: 1.0 Hour 30 Minutes

Full Marks: 75

There are **03** (**Three**) Questions. Answer all of them. Marks in the margin indicate full marks. Don't write on this question paper. Symbols carry their usual meanings. Assume reasonable values for any missing data.

Programmable calculators are not allowed.

-	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	THE RESERVE AND ADDRESS OF		and the second s
	1.	(a)	Consider two identical spherical balls submerged in water at different depths. Will the buoyant forces acting on these two balls be the same or different? Again, consider two 5 cm diameter spherical balls, one made of aluminum, the other of iron, submerged in water. Will the buoyant forces acting on these two balls be the same or different? <i>Explain</i> .	[05] [CO2] [PO2]
		(b)	A typical fluid flow involves a three-dimensional geometry, and the velocity may vary in all three dimensions. Rendering the flow in three-dimensional $V(r, \theta, z)$ in cylindrical coordinates, <i>explain</i> that the fully developed flow in a circular pipe is one-dimensional.	[05] [CO2] [PO2]
		(c)	Express the Bernoulli equation in three different ways using (a) energies, (b) pressures, and (c) heads.	[05] [CO2] [PO2]
	2.	(a)	Derive an expression of viscosity using the principle of Newton's Law of Viscosity. Based on the derivation, differentiate between Newtonian and Non-Newtonian fluid.	[10] [CO3] [PO3]
		(b)	A jet of water strikes tangentially on a smooth curved vane moving in the same direction of the jet. If the vane deflects the jet through an angle of 180° in the opposite direction of the jet. <i>Estimate</i> the value of maximum efficiency.	[10] [CO3] [PO3]
		(c)	Develop an equation for the resultant hydrostatic force acting on the surface and the line of action considering a flat plate completely submerged in a liquid.	[10] [CO3] [PO3]
	3.	(a)	A swimmer having mass of 55 kg is diving in a swimming pool has an effective body area of 0.76 m <sup>2</sup> as shown in <b>Fig.1</b> . The tension in the direction of swimmer's leg is 1.5kN when the legs make an inclination of 30° with the vertical direction. If the swimmer's hands bend about 40° with the flow of water and the magnitude of wave is 2.5 m/s. <i>Calculate</i> the lift and drag forces and their coefficients.	[10] [CO4] [PO4]
		(b)	The pressure of water flowing through a pipe is measured by the arrangement shown in Fig. 2. For the values given, <i>calculate</i> the pressure in the pipe. All the liquids are incompressible. The effect of air column on pressure is negligible.	[10] [CO4] [PO4]
		(c)	A horizontal pipeline is attached to the wall of reservoir ( <b>Fig. 3</b> ). The pipeline has different profiles. The water level in the upper reservoir is in the height $H = 1.5$ m above the pipeline axis. From the lower end of the pipeline water flows out to the open space. Diameters and lengths of pipeline reaches are: $D_1 = 0.24$ m, $L_1 = 3$ m, $D_2 = 0.1$ m, $L_2 = 1$ m, $D_3 = 0.12$ m, $L_3 = 2$ m. Calculate discharge in the pipeline and verify the Bernoulli's equation by drawing the course of EGL and HGL.	[10] [CO4] [PO4]



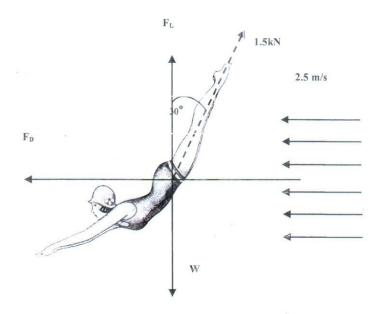


Figure 1: For Question No.3 (a)

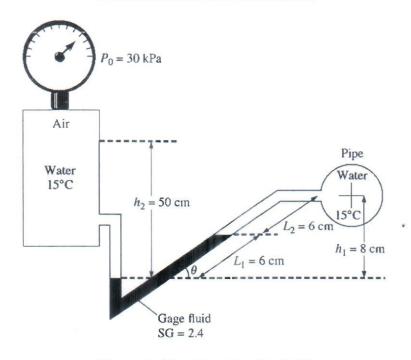


Figure 2: For Question No.3 (b)

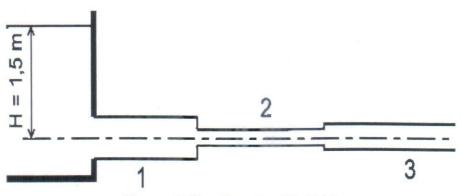


Figure 3: For Question No.3 (c)



Program: B. Sc. in Mechanical Engineering

Semester: 7th

Date: 05 October 2022 (Afternoon)

Time: 2:30 PM - 4:00 PM

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination Course Number: MCE 4709 Course Title: Machine Design II Winter Semester: 2021 - 2022

Full Marks: 50

(PO2, PO3)

Time: 1 Hour 30 Minutes

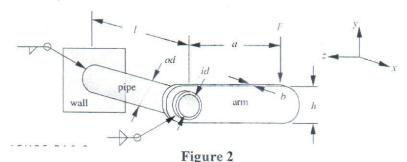
There are **three** questions. Answer **all** of them. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. This is an **OPEN BOOK EXAM** '(Only Textbook allowed, No notes are allowed). Assume reasonable data if necessary. State all assumptions (if any) clearly. Programmable calculators are not allowed.

1. The upside-down steel A frame shown in the **Figure 1** is to be bolted to steel beams on the ceiling of a machine room using bolts. This frame is to support the 50 kN vertical load as shown. The total bolt grip is 48 mm, which includes the thickness of the steel beam, the A-frame feet, and the steel washers used. The frame has two drill holes of 20 mm dia for housing the bolts. <u>Design</u> the joint by selecting a suitable bolt size. The bolt should be of at least ISO 9.8 grade. Justify your design by <u>analyzing</u> the factors of safety guarding against yielding, overload, and joint separation. Also, <u>Determine</u> the tightening torque should be used if the connection is permanent and the fasteners are lubricated.



Figure 1

2. A bracket is welded to a wall as shown in Figure 2 with a fillet weld using an E70 (17) electrode.  $\underline{Design}$  the weld size needed between the tube and wall for a static load F = (CO1) 11 kN and  $h = 1.2 \cdot OD$ ,  $a = 2 \cdot OD$ ,  $l = 2.5 \cdot OD$ . Given that, OD = 89 mm, ID = 78 mm, b = 12.7 mm. The pipe and wall material are made of 1018 HR steel.





(CO2) (PO2) (4)

(CO2)

(PO3)

3. The mean coil diameter of a linear helical compression spring is D = 2.25 inch and the spring index is C = 9. The spring has squared and ground ends and is placed between two flat parallel plates as shown in **Figure 3**. The spring material is music wire A228 and the spring is peened. When the spring is assembled between the plates, the spring at a preload of 45 lbs, the spring length is 5 inches (shown on the left). The spring is then subjected to a fluctuating load. At the maximum working load of 95 lbs, the spring length is 3.75 inches (shown on the right).

### Determine:

- (i) The number of active coils (round up to the nearest quarter of a coil).

  (CO2)

  (PO2)

  (ii) The free length and the shut (solid) height of the spring.

  (CO2)

  (PO2)

  (PO2)

  (PO2)
- (iii) The alternating component and the mean component of the shear stress.
- (iv) The fatigue factor of safety using the Gerber-Zimmerli failure criterion.

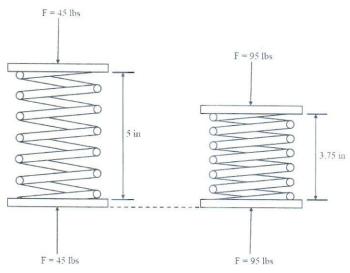


Figure 3



Program: B. Sc. in Mechanical Engineering

# ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC) DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Semester Mid-Semester Examination Course Number: Hum-4717

Course Title: Engineering Economy and Finance

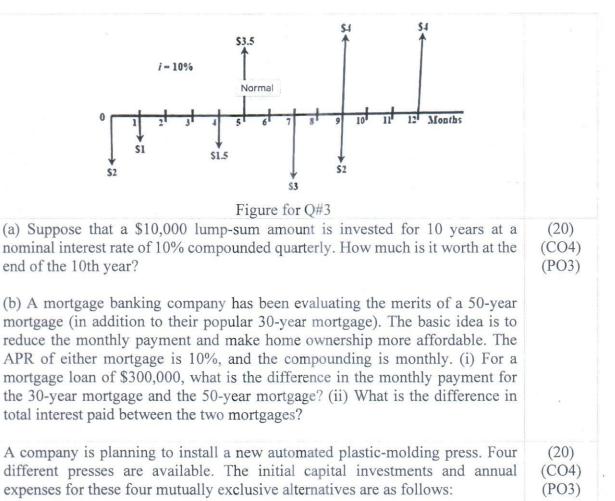
Winter Semester: 2021 - 2022 Full Marks: 75

Time: 1½ hours

There are 5 (five) questions. Answer all of them. Provide cash flow diagram/s whenever applicable. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Necessary formulas and interest tables are provided.

l.	Explain the following terms:  (a) Product life cycle cost	(10) (CO1,2) (PO1)
	<ul> <li>(b) Economic equivalence</li> <li>(c) Minimum Attractive Rate of Return (MARR)</li> <li>(d) Internal Rate of Return (IRR)</li> <li>(e) Discounted payback period</li> </ul>	
2.	Panasonic Inc. produces a lithium-ion battery pack that is used in Electric Vehicles (EVs). The fixed cost is BDT1,000,000 per month, and the variable cost is BDT 10,000 per unit. The selling price per unit is $p = BDT 20,000 - 2(D)$ . For this situation,  (i) determine the optimal volume for maximum revenue and total revenue at this volume  (ii) determine the optimal volume for this product for maximum profit; total revenue and profit at this volume  (iii) find the volumes at which breakeven occurs  (iv) draw demand vs. revenue, fixed cost, and variable cost curve; show volumes for maximum revenue and profit, breakeven points and profit area for this case.	v 1
4	Cash flow diagram of a 12-month industrial project (in units of \$1,000,000) is shown in the following figure (Fig Q#3). Assume a nominal interest rate of 12% compounded monthly. Calculate  (a) Present equivalent of all investment amounts (cash out flows)  (b) Present equivalent of all revenues (cash inflows)  (c) Present equivalent of all cash flows	(10) (CO3) (PO3)





	P1	P2	P3	. P4
Capital investment	\$24,000	\$30,400	\$49,600	\$52,000
Useful life (years)	5	5	10	10
Annual expenses (\$):				
Power	2,720	2,720	4,800	5,040
Labor	26,400	24,000	16,800	14,800
Maintenance	1,600	1,800	2,600	2,000
Property taxes	480	608	992	1,040

Assume that each press has the same output capacity (120,000 units per year) and has no market value at the end of its useful life and any additional capital investment is expected to earn at least 10% per year. Which press should be chosen if 120,000 non-defective units per year are produced by each press and all units can be sold? The selling price is \$0.5 per unit.



Program: B. Sc. in Mechanical Engineering

Semester: Winter

Date: 30 September, 2022 Time: 2:30 pm – 4:00 pm

## ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Semester Mid Examination

Course Number: MCE 4721

Course Title: Manufacturing System and Automation

Winter Semester: 2021 - 2022

Full Marks: 75

Time: 1.5 Hours

There are 3 (**THREE**) questions. Answer 3 (**THREE**) questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in the brackets. Answer either Part A or Part B of Question 3. A Formula sheet is provided.

1. Discuss current realities of manufacturing activities at global (10 Marks) perspective. (CO1)(PO) b. Elaborate on significant of Manufacturing System that is a (15 Marks) component of Production System to overall performances in (CO1)production. (PO) 2. As a technical manager of a textile manufacturing company, you are a. (CO1)tasked with improving the production efficiency. (PO 1) Suggest and elaborate on FIVE (5) strategies for production improvement via implementation of automation technologies. (15 Marks) b. Manufacturing companies often attempt to organize its facilities in the (CO 1) most efficient way to serve the particular mission of the plant. (PO 1) Discuss the strategies for production facilities based on product (10 Marks) variety and quantity.

### 3. ANSWERS EITHER PART A OR PART B

### PART A

a. An automotive part undergoes through six machines in a batch (CO 2) production plant. Table 1 lists the setup and operation times of each (PO 2) machine. Consider a batch size of 200 with average nonoperation time per machine of 6 hours.

### Solve for:

i. Manufacturing lead time.

(10 Marks)

ii. Production rate for machine 3. (5 Marks)

Table 1: Setup time and operation time

Machine	Setup time	Operation time		
	(hr.)	(min.)		
1	2	5.0		
2	4	3.5		
3	6	10.0		
4	1	1.9		
5	2	4.1		
6	4	2.5		

b. An improvement is made to the previous operation whereby an (CO 2) automated work handling system is used to transfer parts between (PO 2) machines. The transfer time between stations equals 10s while the total time to set up the entire line is 100 hours. Assume that the operation times at the individual machines remain the same.

Solve for,

i. Manufacturing lead time.

(4 Marks)

ii. Production rate for machine 3.

(3 Marks)

iii. Comments on results in (a) and (b).

(3 Marks)

#### PART B

a. A Dhaka Limited Company plans to introduce a new product line. The product line consists of 25 different models. Annual production of (PO 2) each model is expected to be 500 units with each product consists of 100 components. There are an average of 6 processing steps required to produce each component, and each processing step takes 2.0 minute (includes an allowance for setup time and part handling). All processing operations are performed at workstations, each of which includes a production machine and a human worker. Each workstation requires a floor space of 200 m², and the factory operates on one shift which is equivalent to 2000 hr/yr.

Solve for,

i.	number of production	on operations (opt/yr).	(4 Marks)

ii. number of workers requirement. (5 Marks)

iii. floorspace are requirement. (6 Marks)

b. A further development on the part design is desired for the production setup in (a). Products are assembled on the single workstations consisting of two workers each. Each final unit of the product will takes 3.0 hours to assemble.

Solve for,

i.	number of workers requirement.	(4 Marks)
ii.	floorspace are requirement.	(3 Marks)
iii.	comments on results obtained in (a) and (b)	(3 Marks)

### FORMULA SHEET

$$T_c = T_o + T_h + T_{th}$$

$$T_b = T_{su} + QT_c$$

$$R_p = 1/T_p$$

$$PC_w = n S_w H_s R_p$$

$$PC_{w} = \frac{nS_{w}H_{s}R_{p}}{n_{o}}$$

$$U = Q / PC$$

$$A = (MTBF - MTTR) / MTBF$$

$$MLT = n_o (T_{su} + QT_c + T_{no})$$



Program: B.Sc. Engg. (ME) 7<sup>th</sup> Sem / B.Sc.TE 3<sup>rd</sup> Sem Date: 03 October, 2022

Semester: Winter semester

(Afternoon)

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT)

ORGANISATION OF ISLAMIC COOPERATION (OIC) DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

**Mid Semester Examination** 

Course Number: MCE 4729/93

Course Title: Production and Operations Management

Winter Semester: 2021 – 2022

Full Marks: 75

[10]

[CO1]

[PO2]

Time: 1.5 Hours

There are 3 (three) questions. Answer all questions. The symbols have their usual meanings. Marks of each question and corresponding CO and PO are written in square brackets. Assume a reasonable value for missing data. Programmable calculators are not allowed.

(a) The Instant Paper Clip Office Supply Company sells and delivers office 1. supplies to companies, schools, and agencies within a 50-mile radius of its warehouse. The office supply business is competitive, and the ability to deliver orders promptly is a significant factor in getting new customers and maintaining old ones. (Offices typically order not when they run low on supplies but when they completely run out; as a result, they need their orders immediately.) The company's manager wants to ensure enough drivers and vehicles are available to deliver orders promptly and have adequate inventory in stock. Therefore, the manager wants to be able to forecast the demand for deliveries during the next month. From the records of previous orders, management has accumulated the following data for the past ten months:

Month	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.
Orders	120	90	100 -	75	110	50	75	130	110	90

- i. Compute the monthly demand forecast for April through November using a 3-month moving average.
- ii. Compute the monthly demand forecast for June through November using a 5-month moving average.
- iii. Compute the monthly demand forecast for April through November using a 3-month weighted moving average. Use weights of 0.5, 0.33, and 0.17, with heavier weights in the more recent months.
- iv. Compute the mean absolute deviation for June through October for each method used. Which method would you use to forecast demand for November?

(b) PM Computer Services assembles customized personal computers from generic parts. Formed and operated by part-time UMass Lowell students Paulette Tyler and Maureen Becker, the company has had steady growth since it started. The company assembles computers mostly at night, using part-time students. Paulette and Maureen purchase generic computer parts in volume at a discount from a variety of sources whenever they see a good deal. Thus, they need a good forecast of demand for their computers so that they will know how

[15] [CO1] [PO2]



many parts to purchase and stock. They have compiled demand data for the last 12 months, as reported below.

Period	Month	Demand	Period	Month	Demand
1	January	37	7	July	43
2	February	40	8	August	47
3	March	41	9	September	56
4	April	37	10	October	52
5	May	45	11	November	55
6	June	50	12	December	54

- i. Use exponential smoothing with smoothing parameter  $\alpha = 0.3$  to compute the demand forecast for January (Period 13).
- ii. Use exponential smoothing with smoothing parameter  $\alpha = 0.5$  to compute the demand forecast for January (Period 13).
- iii. Paulette believes that there is an upward trend in the demand. Use trend-adjusted exponential smoothing with smoothing parameter  $\alpha = 0.5$  and trend parameter  $\beta = 0.3$  to compute the demand forecast for January (Period 13).
- iv. Compute the mean squared error for each method used and comment on the results.
- 2. (a) An auto parts supplier sells Hardy-brand batteries to car dealers and auto mechanics. The annual demand is approximately 1,200 batteries. The supplier pays \$28 for each battery and estimates that the annual holding cost is 30 percent of the battery's value. It costs approximately \$20 to place an order (managerial and clerical costs). The supplier currently orders 100 batteries per month.

[10] [CO1] [PO2]

- i. Determine the ordering, holding, and total inventory costs for the current order quantity.
- ii. Determine the economic order quantity (EOQ).
- iii. How many orders will be placed per year using the EOQ?
- iv. Determine the ordering, holding, and total inventory costs for the *EOQ*.
- v. How has ordering cost changed? Holding cost? Total inventory cost?
- (b) Upon closer inspection, the supplier determines that the demand for batteries is normally distributed with a mean of 4 batteries per day and a standard deviation of 3 batteries per day. (The supplier is open 300 days per year.) It usually takes about 4 days to receive an order from the factory.

[15] [CO1] [PO2]

- i. What is the standard deviation of usage during the lead time?
- ii. Determine the reorder point needed to achieve a service level of 95 percent.
- iii. What is the safety stock? What is the holding cost associated with this safety stock?
- iv. How would your analysis change if the service level changed to 98 percent?

3. (a) An organization is considering two different locations for a new plant. They request a consulting firm to study the sites. In their board meeting, the organization decided that the following five factors may be considered. The consulting firm submitted the result of their study in the table given below. What site will be preferable?

[10] [CO2] [PO3/ PO5]

Sl. No. Location		Weight	Score		
	Location Factor		Location 1	Location 2	
1.	1. Facility Utilization		3	3	
2.	Total load km per month	15	5	5	
3.	Average time for delivery	30	4	4	
4.	Land and construction costs	20	2	2	
5.	Employee preference	10	5	4	

(b) You're an analyst for a renowned organization. The organization is considering a new manufacturing plant in Rajshahi, Dhaka, Comilla, or Chittagong. Fixed costs per year are \$30k, \$100k, \$60k, and \$110k, respectively. Variable costs per product are \$45, \$75, & \$35, and \$60, respectively. Identify the range in volume over which each location would be best. If the price per product is \$150, \$120, \$100, and \$90, respectively, and forecast demand per year is 20k, 50k, 30k, and 40k, respectively, then determine the best site.

[15] [CO2] [PO3/ PO5]



(15) (CO1)

(PO2)

(10) (CO1)

(PO2)

(13) (CO1)

(PO2)

(12) (CO1)

(PO2)

(18)

(CO2)

(PO2)

Program: B.Sc. Engg. (ME)

Semester: 7th Sem.

Date: 30 September 2022 Time: 02:30 pm - 04:00 pm

### ISLAMIC UNIVERSITY OF TECHNOLOGY (IUT) ORGANISATION OF ISLAMIC COOPERATION (OIC)

### DEPARTMENT OF MECHANICAL AND PRODUCTION ENGINEERING

Mid Semester Examination

Course No.: MCE 4787

Course Title: Automobile Engineering

Winter Semester, A. Y. 2021-2022

Time: 1 Hours 30 Min(s)

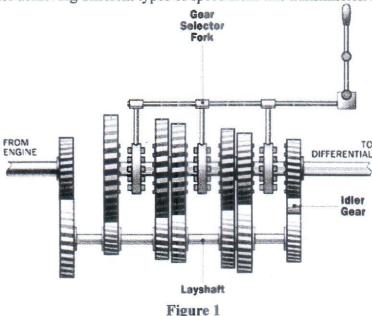
Full Marks: 75

There are 3 (Three) questions. Answer all the questions.

Marks of each question and corresponding CO and PO are written in the brackets.

Do not write on this question paper.

- 1. a) Classify automobile chassis? Briefly explain the different components of an automobile chassis.
  - b) Why mixture correction is necessary for a carburetor operation? Explain how you can achieve mixture correction by using an air bleed.
- 2. a) How a catalytic converter converts the harmful exhaust gases to less toxic mixture of carbon dioxide  $(CO_2)$ , Nitrogen  $(N_2)$  and Water vapors  $(H_2O)$  in its different stages. Explain with necessary diagrams and chemical reactions.
  - b) It is known that an engine is very powerful for its size if it can produce 100 HP per liter of displacement. However, this efficiency goal is harder to accomplish. To achieve this goal, what are the specific technologies commonly used? Explain any one of them.
- a) A manual transmission gearbox is shown in Figure 1. Explain the necessary connecting arrangement for achieving different types of speed from this transmission system.



b) Explain the necessity of synchronizer in the transmission system shown in Figure 1.

(7) (CO2) (PO2)